



TISP4015H1BJ, TISP4025H1BJ, TISP4030H1BJ, TISP4040H1BJ

## VERY LOW VOLTAGE BIDIRECTIONAL THYRISTOR OVERVOLTAGE PROTECTORS

### TISP40xxH1BJ VLV Overvoltage Protector Series

#### Low Capacitance

'4015.....	78 pF
'4030.....	62 pF
'4040.....	59 pF

#### Digital Line Signal Level Protection

-ISDN  
-xDSL

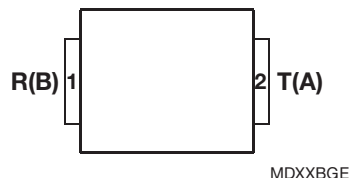
#### Safety Extra Low Voltage, SELV, values

Device	V <sub>DRM</sub> V	V <sub>(BO)</sub> V
'4015	± 8	± 15
'4025	± 13	± 25
'4030	± 15	± 30
'4040	± 25	± 40

100 A "H" Series specified for:  
ITU-T recommendations K.20, K.45, K.21  
FCC Part 68 and GR-1089-CORE

Wave Shape	Standard	I <sub>TSP</sub> A
2/10 μs	GR-1089-CORE	500
8/20 μs	IEC 61000-4-5	400
10/160 μs	FCC Part 68	200
10/700 μs	ITU-T K.20/45/21 FCC Part 68	150
10/560 μs	FCC Part 68	125
10/1000 μs	GR-1089-CORE	100

#### SMBJ Package (Top View)



#### Device Symbol



Terminals T and R correspond to the  
alternative line designators of A and B

 ..... **UL Recognized Components\*\***

#### Description

These devices are designed to limit overvoltages on digital telecommunication lines. Overvoltages are normally caused by a.c. power system or lightning flash disturbances which are induced or conducted on to the telephone line. A single device provides 2-point protection and is typically used for the protection of transformer windings and low voltage electronics.

The protector consists of a symmetrical voltage-triggered bidirectional thyristor. Overvoltages are initially clipped by breakdown clamping until the voltage rises to the breakover level, which causes the device to crowbar into a low-voltage on-state condition. This low-voltage on state causes the current resulting from the overvoltage to be safely diverted through the device. The device switches off when the diverted current falls below the holding current value.

#### How to Order

Device	Package	Carrier	Order As	Marking Code	Std. Qty.
TISP40xxH1BJ	SMB (DO-214AA)	Embossed Tape Reeled	TISP 40xxH1BJR-S	40xxH1	3000

Insert xx value corresponding to protection voltages of 15 V, 30 V and 40 V.

\*RoHS Directive 2002/95/EC Jan. 27, 2003 including annex and RoHS Recast 2011/65/EU June 8, 2011.

\*\* TISP4025H1BJ UL Recognition pending.

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## Absolute Maximum Ratings, $T_A = 25^\circ\text{C}$ (Unless Otherwise Noted)

Rating	Symbol	Value	Unit
Repetitive peak off-state voltage	$V_{\text{DRM}}$	$\pm 8$ $\pm 13$ $\pm 15$ $\pm 25$	V
Non-repetitive peak on-state pulse current (see Notes 1 and 2) 2/10 $\mu\text{s}$ (Telcordia GR-1089-CORE, 2/10 $\mu\text{s}$ voltage wave shape) 8/20 $\mu\text{s}$ (IEC 61000-4-5, combination wave generator, 1.2/50 voltage, 8/20 current) 10/160 $\mu\text{s}$ (FCC Part 68, 10/160 $\mu\text{s}$ voltage wave shape) 5/310 $\mu\text{s}$ (ITU-T K.20/45/21, 10/700 $\mu\text{s}$ voltage wave shape) 5/320 $\mu\text{s}$ (FCC Part 68, 9/720 $\mu\text{s}$ voltage wave shape) 10/560 $\mu\text{s}$ (FCC Part 68, 10/560 $\mu\text{s}$ voltage wave shape) 10/1000 $\mu\text{s}$ (Telcordia GR-1089-CORE, 10/1000 $\mu\text{s}$ voltage wave shape)	$I_{\text{TSP}}$	$\pm 500$ $\pm 400$ $\pm 200$ $\pm 150$ $\pm 150$ $\pm 125$ $\pm 100$	A
Non-repetitive peak on-state current (see Notes 1 and 2) 20 ms (50 Hz) full sine wave 16.7 ms (60 Hz) full sine wave 0.2 s 50 Hz/60 Hz a.c. 2 s 50 Hz/60 Hz a.c. 1000 s 50 Hz/60 Hz a.c.	$I_{\text{TSM}}$	45 50 21 7 2	A
Initial rate of rise of current (2/10 waveshape)	$di/dt$	450	A/ $\mu\text{s}$
Junction temperature	$T_J$	-40 to +150	$^\circ\text{C}$
Storage temperature range	$T_{\text{stg}}$	-65 to +150	$^\circ\text{C}$

NOTES: 1. Initially the device must be in thermal equilibrium with  $T_J = 25^\circ\text{C}$ .  
 2. The surge may be repeated after the device returns to its initial conditions.

## Electrical Characteristics, $T_A = 25^\circ\text{C}$ (Unless Otherwise Noted)

Parameter	Test Conditions	Min	Typ	Max	Unit
$I_{\text{DRM}}$ Repetitive peak off-state current	$V_D = V_{\text{DRM}}$			$\pm 5$	$\mu\text{A}$
$V_{(\text{BO})}$ Breakover voltage	$di/dt = 0.8 \text{ A/ms}$			$\pm 15$ $\pm 25$ $\pm 30$ $\pm 40$	V
$V_{(\text{BO})}$ Impulse breakover voltage	$dv/dt \leq \pm 1000 \text{ V}/\mu\text{s}$ , Linear voltage ramp, Maximum ramp value = $\pm 500 \text{ V}$ $di/dt = \pm 12 \text{ A}/\mu\text{s}$ , Linear current ramp, Maximum ramp value = $\pm 10 \text{ A}$			$\pm 33$ $\pm 57$ $\pm 74$	V
$I_{(\text{BO})}$ Breakover current	$di/dt = \pm 0.8 \text{ A/ms}$			$\pm 0.8$	A
$V_T$ On-state voltage	$I_T = \pm 5 \text{ A}$ , $t_w = 100 \mu\text{s}$			$\pm 3$	V
$I_D$ Off-state current	$V_D = \pm 6 \text{ V}$ $V_D = \pm 11 \text{ V}$ $V_D = \pm 13 \text{ V}$ $V_D = \pm 22 \text{ V}$			$\pm 2$	$\mu\text{A}$
$I_H$ Holding current	$I_T = \pm 5 \text{ A}$ , $di/dt = \pm 30 \text{ mA/ms}$	$\pm 50$			m A

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## Electrical Characteristics, $T_A = 25\text{ }^{\circ}\text{C}$ (Unless Otherwise Noted)

Parameter	Test Conditions	Min	Typ	Max	Unit
$C_{off}$ Off-state capacitance	$f = 1\text{ MHz}, V_d = 1\text{ V rms}, V_D = 0$		'4015	78	100
			'4025 / '4030	62	81
			'4040	59	77
	$f = 1\text{ MHz}, V_d = 1\text{ V rms}, V_D = 1\text{ V}$		'4015	70	90
			'4025 / '4030	55	72
			'4040	52	68
	$f = 1\text{ MHz}, V_d = 1\text{ V rms}, V_D = 2\text{ V}$		'4015	65	85
			'4025 / '4030	50	65
			'4040	47	61

## Thermal Characteristics

Parameter	Test Conditions	Min	Typ	Max	Unit
$R_{\theta JA}$ Junction to free air thermal resistance	EIA/JESD51-3 PCB, $I_T = I_{TSM(1000)}$ , $T_A = 25\text{ }^{\circ}\text{C}$ , (see Note 3)			115	$^{\circ}\text{C/W}$
	265 mm x 210 mm populated line card, 4-layer PCB, $I_T = I_{TSM(1000)}$ , $T_A = 25\text{ }^{\circ}\text{C}$		52		

NOTE 3: EIA/JESD51-2 environment and PCB has standard footprint dimensions connected with 5 A rated printed wiring track widths.

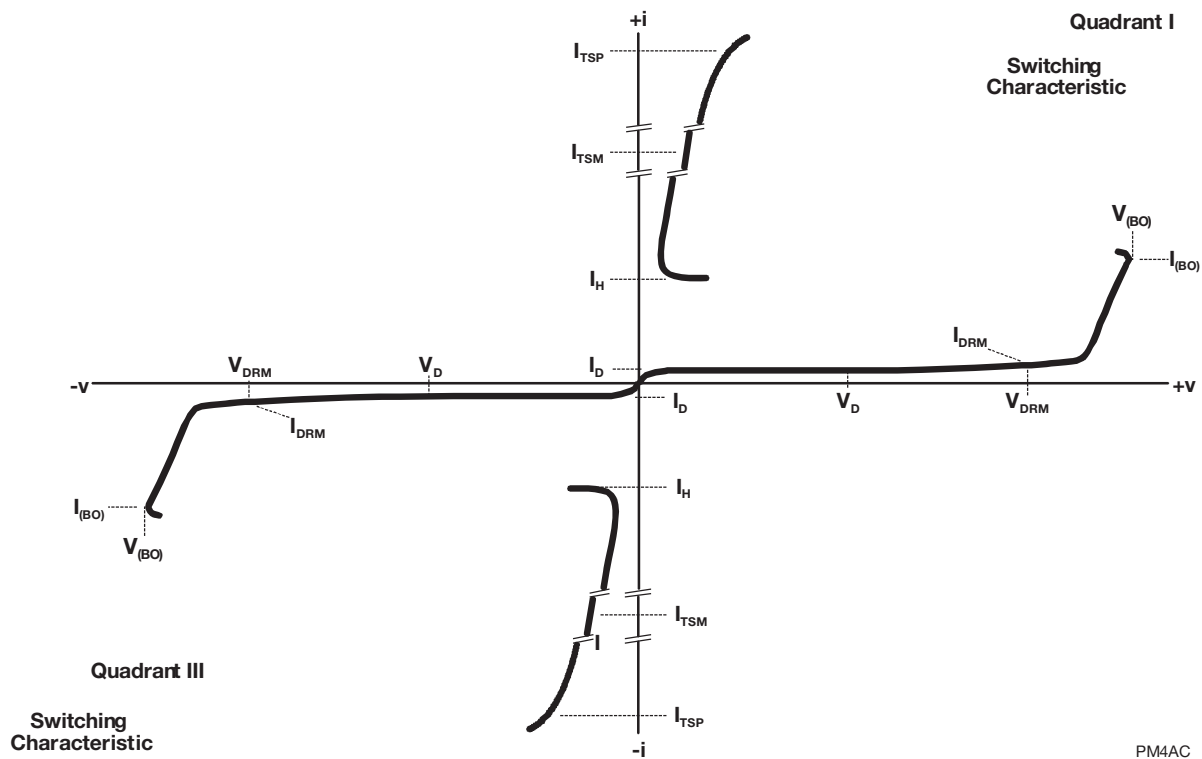
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## Parameter Measurement Information



**Figure 1. Voltage-Current Characteristic for T and R Terminals**  
**All Measurements are Referenced to the R Terminal**

## Typical Characteristics

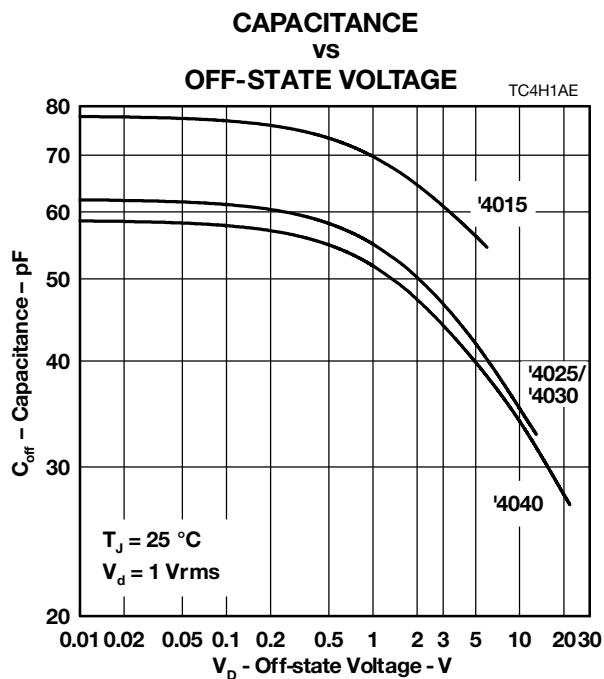
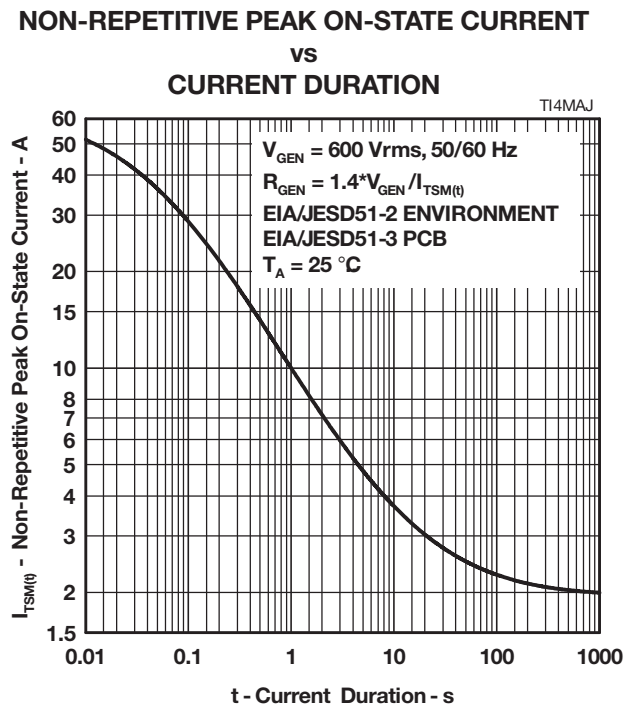


Figure 2.

## Rating and Thermal Information



**Figure 3.**

## APPLICATIONS INFORMATION

### Transformer Protection

The inductance of a transformer winding reduces considerably when the magnetic core material saturates. Saturation occurs when the magnetizing current through the winding inductance exceeds a certain value. It should be noted that this is a different current to the transformed current component from primary to secondary. The standard inductance-current relationship is:

$$E = -\left(L \frac{di}{dt}\right)$$

where:

$L$  = unsaturated inductance value in H

$di$  = current change in A

$dt$  = time period in s for current change  $di$

$E$  = winding voltage in V

Rearranging this equation and working large  $\Delta$  changes to saturation gives the useful circuit relationship of:

$$E \times \Delta t = L \times \Delta i$$

A transformer winding volt-second value for saturation gives the designer an idea of circuit operation under overvoltage conditions. The volt-second value is not normally quoted, but most manufacturers should provide it on request. A  $50 \text{ V}\mu\text{s}$  winding will support rectangular voltage pulses of 50 V for 1  $\mu\text{s}$ , 25 V for 2  $\mu\text{s}$ , 1 V for 50  $\mu\text{s}$  and so on. Once the transformer saturates, primary to secondary coupling will be lost and the winding resistance,  $R_W$ , shunts the overvoltage protector, Th1 - see Figure 4. This saturated condition is a concern for long duration impulses and a.c. fault conditions because the current capability of the winding wire may be exceeded. For example, if the on-state voltage of the protector is 1 V and the winding resistance is 0.2  $\Omega$ , the winding would bypass a current of  $1/0.2 = 5 \text{ A}$ , even through the protector was in the low voltage condition.



Figure 4. Transformer Saturation

Figure 5 shows a generic protection arrangement. Resistors R1 and R2, together with the overcurrent protection, prevent excessive winding current flow under a.c. conditions. Normally these resistors would only be needed for special cases, e.g. some T1/E1 designs. Alternatively, a split winding could be used with a single resistor connecting the windings. This resistor could be by-passed by a small capacitor to reduce signal attenuation.

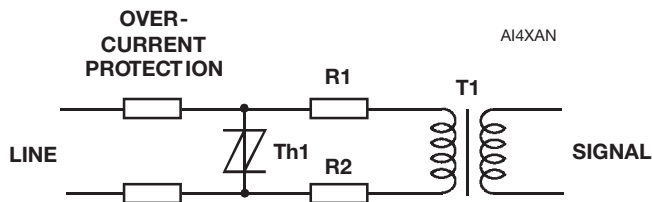


Figure 5. Transformer Winding Protection

Overcurrent protection upstream from the overvoltage protector can be fuse, PTC or thick film resistor based. For very high frequency circuits, fuse inductance due to spiral wound elements may need to be evaluated.

### TISP® Device Voltage Selection

Normally, the working voltage value of the protector,  $V_{\text{DRM}}$ , would be chosen to be just greater than the peak signal amplitude over the equipment temperature range. This would give the lowest possible protection voltage,  $V_{\text{BO}}$ . This would minimize the peak voltage applied to the transformer winding and increase the time to core saturation.

In high frequency circuits, there are two further considerations. Low voltage protectors have a higher capacitance than high voltage protectors.

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## TISP® Device Voltage Selection (Continued)

So a higher voltage protector might be chosen specifically to reduce the protector capacitive effects on the signal.

Low energy short duration spikes will be clipped by the protector. This will extend the spike duration and the data loss time. A higher protector voltage will reduce the data loss time. Generally, this will not be a significant factor for inter-conductor protection.

However, clipping is significant for protection to ground, where there is continuous low-level a.c. common mode induction. In some cases the induced a.c. voltage can be over 10 V. Repetitive clipping at the induced a.c. peaks by the protector would cause severe data corruption. The expected a.c. voltage induced should be added to the maximum signal level for setting the protector  $V_{DRM}$  value.

## 2-Wire Digital Systems

Typical systems using a single twisted pair connection are: Integrated Services Digital Network (ISDN) and Pair Gain.

Signal level protection at the transformer winding is given by protectors Th3 and Th5. Typically these could be TISP4015H1 type devices with a 15 V voltage protection level.

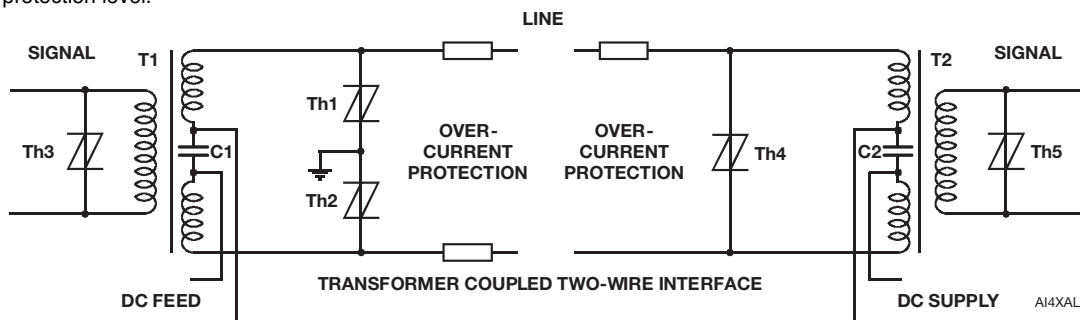


Figure 6. 2-Wire System

Two line protection circuits are given; one referenced to ground using Th1 and Th2 (left) and the other inter-wire using protector Th4 (right) - see Figure 6. For ISDN circuits compliant to ETSI ETR 080:1993, ranges 1 and 2 can be protected by the following device types: TISP4095M3, TISP4095H3, TISP3095H3 (combines Th1 and Th2) and TISP7095H3 (combines Th1, Th2 and Th4). Ranges 4 through 5 can be protected by: TISP4145M3, TISP4145H3, TISP3145H3 (combines Th1 and Th2) and TISP7145H3 (combines Th1, Th2 and Th4). Device surge requirement, H or M, will be set by the overcurrent protection components and the standards complied with. Protection of just the d.c. feed to ETSI ranges is covered in the TISP5xxxH3 data sheet.

When loop test voltages exceed the normal d.c. feed levels, higher voltage protectors need to be selected. For two terminal protectors, for levels up to 190 V (135 V rms) the TISP4250, H3 or M3, can be used and for 210 V (150 V rms) the TISP4290, H3 or M3, can be used.

In Pair Gain systems, the protector  $V_{DRM}$  is normally set by the d.c. feed value. The following series of devices have a 160 V working voltage at 25 °C: TISP4220M3, TISP4220H3, TISP3210H3 (combines Th1 and Th2) and TISP7210H3 (combines Th1, Th2 and Th4). These devices can be used on 150 V d.c. feed voltages down to an ambient temperature of -25 °C. Where the subscriber equipment may be exposed to POTS (Plain Old Telephone Service) voltage levels, protector Th4 needs a higher working voltage of about 275 V. Suitable device types are: TISP4350M3, TISP4350H3, TISP3350H3 (combines Th1 and Th2) and TISP7350H3 (combines Th1, Th2 and Th4).

The overcurrent protection for the overvoltage protector can be fuse, PTC or thick film resistor based. Its a.c. limiting capability should be less than the ratings of the intended overvoltage protector. Equipment complying with the year 2000 international K.20, K.21 and K.45 recommendations from the ITU-T, may be required to demonstrate protection coordination with the intended primary protector. Without adding series resistance, a simple series fuse overcurrent protection is likely to fail the equipment for this part of the recommendation.

If the d.c. feed consists of equal magnitude positive and negative voltage supplies, appropriately connected TISP5xxxH3 unidirectional protectors could replace Th1 and Th2.

## 4-Wire Digital Systems

A typical system using a two twisted pair connection is the High-bit-rate Digital Subscriber Line (HDSL) and the "S" interface of ISDN.

Figure 7 shows a generic two line system. HDSL tends to have ground referenced protection at both ends of the lines (Th1, Th2, Th3 and Th4). The ISDN "S" interface is often inside the premises and simple inter-wire protection is used at the terminating adaptor (Th7 and Th8). In all

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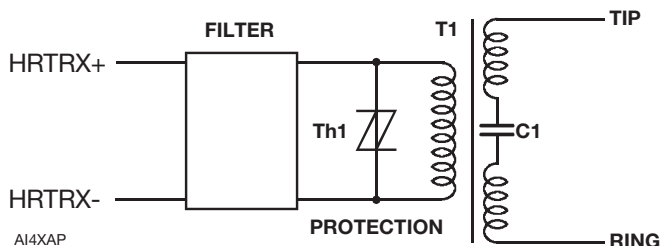
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### Figure 7. 4-Wire System



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