

# 1N5817, 1N5818, 1N5819

1N5817 and 1N5819 are Preferred Devices

## Axial Lead Rectifiers

This series employs the Schottky Barrier principle in a large area metal-to-silicon power diode. State-of-the-art geometry features chrome barrier metal, epitaxial construction with oxide passivation and metal overlap contact. Ideally suited for use as rectifiers in low-voltage, high-frequency inverters, free wheeling diodes, and polarity protection diodes.

### Features

- Extremely Low  $V_F$
- Low Stored Charge, Majority Carrier Conduction
- Low Power Loss/High Efficiency
- These are Pb-Free Devices\*

### Mechanical Characteristics:

- Case: Epoxy, Molded
- Weight: 0.4 Gram (Approximately)
- Finish: All External Surfaces Corrosion Resistant and Terminal Leads are Readily Solderable
- Lead Temperature for Soldering Purposes:  
260°C Max for 10 Seconds
- Polarity: Cathode Indicated by Polarity Band
- ESD Ratings: Machine Model = C (>400 V)  
Human Body Model = 3B (>8000 V)



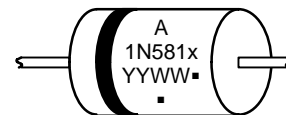
**ON Semiconductor®**

<http://onsemi.com>

**SCHOTTKY BARRIER  
RECTIFIERS  
1.0 AMPERE  
20, 30 and 40 VOLTS**



### MARKING DIAGRAM



A =Assembly Location  
1N581x =Device Number  
x= 7, 8, or 9  
YY =Year  
WW =Work Week  
▪ =Pb-Free Package

(Note: Microdot may be in either location)

### ORDERING INFORMATION

See detailed ordering and shipping information on page 6 of this data sheet.

**Preferred** devices are recommended choices for future use and best overall value.

\*For additional information on our Pb-Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

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## MAXIMUM RATINGS

Rating	Symbol	1N5817	1N5818	1N5819	Unit
Peak Repetitive Reverse Voltage Working Peak Reverse Voltage DC Blocking Voltage	$V_{RRM}$ $V_{RWM}$ $V_R$	20	30	40	V
Non-Repetitive Peak Reverse Voltage	$V_{RSM}$	24	36	48	V
RMS Reverse Voltage	$V_{R(RMS)}$	14	21	28	V
Average Rectified Forward Current (Note 1), ( $V_{R(equiv)} \leq 0.2 V_R(dc)$ , $T_L = 90^\circ C$ , $R_{\theta JA} = 80^\circ C/W$ , P.C. Board Mounting, see Note 2, $T_A = 55^\circ C$ )	$I_O$	1.0			A
Ambient Temperature (Rated $V_R(dc)$ , $P_{F(AV)} = 0$ , $R_{\theta JA} = 80^\circ C/W$ )	$T_A$	85	80	75	$^\circ C$
Non-Repetitive Peak Surge Current, (Surge applied at rated load conditions, half-wave, single phase 60 Hz, $T_L = 70^\circ C$ )	$I_{FSM}$	25 (for one cycle)			A
Operating and Storage Junction Temperature Range (Reverse Voltage applied)	$T_J, T_{stg}$	-65 to +125			$^\circ C$
Peak Operating Junction Temperature (Forward Current applied)	$T_{J(pk)}$	150			$^\circ C$

Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Recommended Operating Conditions may affect device reliability.

## THERMAL CHARACTERISTICS (Note 1)

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction-to-Ambient	$R_{\theta JA}$	80	$^\circ C/W$

## ELECTRICAL CHARACTERISTICS ( $T_L = 25^\circ C$ unless otherwise noted) (Note 1)

Characteristic	Symbol	1N5817	1N5818	1N5819	Unit
Maximum Instantaneous Forward Voltage (Note 2)	$v_F$	0.32	0.33	0.34	V
	( $i_F = 0.1 A$ )				
	( $i_F = 1.0 A$ )	0.45	0.55	0.6	
	( $i_F = 3.0 A$ )	0.75	0.875	0.9	
Maximum Instantaneous Reverse Current @ Rated dc Voltage (Note 2)	$I_R$	1.0	1.0	1.0	mA
	( $T_L = 25^\circ C$ )				
	( $T_L = 100^\circ C$ )	10	10	10	

1. Lead Temperature reference is cathode lead 1/32 in from case.
2. Pulse Test: Pulse Width = 300  $\mu s$ , Duty Cycle = 2.0%.

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## NOTE 3. — DETERMINING MAXIMUM RATINGS

Reverse power dissipation and the possibility of thermal runaway must be considered when operating this rectifier at reverse voltages above  $0.1 V_{RWM}$ . Proper derating may be accomplished by use of equation (1).

$$T_{A(max)} = T_{J(max)} - R_{\theta JA} P_{F(AV)} - R_{\theta JA} P_{R(AV)} \quad (1)$$

where  $T_{A(max)}$  = Maximum allowable ambient temperature  
 $T_{J(max)}$  = Maximum allowable junction temperature (125°C or the temperature at which thermal runaway occurs, whichever is lowest)  
 $P_{F(AV)}$  = Average forward power dissipation  
 $P_{R(AV)}$  = Average reverse power dissipation  
 $R_{\theta JA}$  = Junction-to-ambient thermal resistance

Figures 1, 2, and 3 permit easier use of equation (1) by taking reverse power dissipation and thermal runaway into consideration. The figures solve for a reference temperature as determined by equation (2).

$$T_R = T_{J(max)} - R_{\theta JA} P_{R(AV)} \quad (2)$$

Substituting equation (2) into equation (1) yields:

$$T_{A(max)} = T_R - R_{\theta JA} P_{F(AV)} \quad (3)$$

Inspection of equations (2) and (3) reveals that  $T_R$  is the ambient temperature at which thermal runaway occurs or where  $T_J = 125^\circ\text{C}$ , when forward power is zero. The transition from one boundary condition to the other is evident on the curves of Figures 1, 2, and 3 as a difference in the rate of change of the slope in the vicinity of  $115^\circ\text{C}$ . The data of Figures 1, 2, and 3 is based upon dc conditions. For use in common rectifier circuits, Table 1 indicates suggested factors for an equivalent dc voltage to use for conservative design, that is:

$$V_{R(equiv)} = V_{in(PK)} \times F \quad (4)$$

The factor F is derived by considering the properties of the various rectifier circuits and the reverse characteristics of Schottky diodes.

EXAMPLE: Find  $T_{A(max)}$  for 1N5818 operated in a 12-volt dc supply using a bridge circuit with capacitive filter such that  $I_{DC} = 0.4 \text{ A}$  ( $I_{F(AV)} = 0.5 \text{ A}$ ),  $I_{(FM)}/I_{(AV)} = 10$ , Input Voltage =  $10 V_{(rms)}$ ,  $R_{\theta JA} = 80^\circ\text{C/W}$ .

Step 1. Find  $V_{R(equiv)}$ . Read  $F = 0.65$  from Table 1,

$$\therefore V_{R(equiv)} = (1.41)(10)(0.65) = 9.2 \text{ V}$$

Step 2. Find  $T_R$  from Figure 2. Read  $T_R = 109^\circ\text{C}$

@  $V_R = 9.2 \text{ V}$  and  $R_{\theta JA} = 80^\circ\text{C/W}$ .

Step 3. Find  $P_{F(AV)}$  from Figure 4. \*\*Read  $P_{F(AV)} = 0.5 \text{ W}$

$$\text{@ } \frac{I_{(FM)}}{I_{(AV)}} = 10 \text{ and } I_{F(AV)} = 0.5 \text{ A.}$$

Step 4. Find  $T_{A(max)}$  from equation (3).

$$T_{A(max)} = 109 - (80)(0.5) = 69^\circ\text{C}.$$

\*\*Values given are for the 1N5818. Power is slightly lower for the 1N5817 because of its lower forward voltage, and higher for the 1N5819.

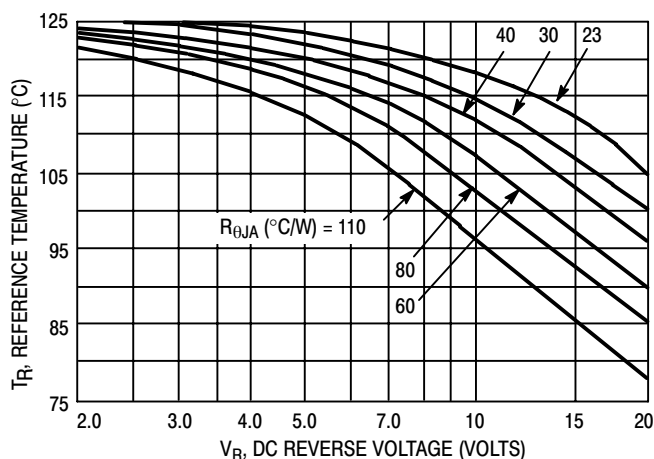


Figure 1. Maximum Reference Temperature 1N5817

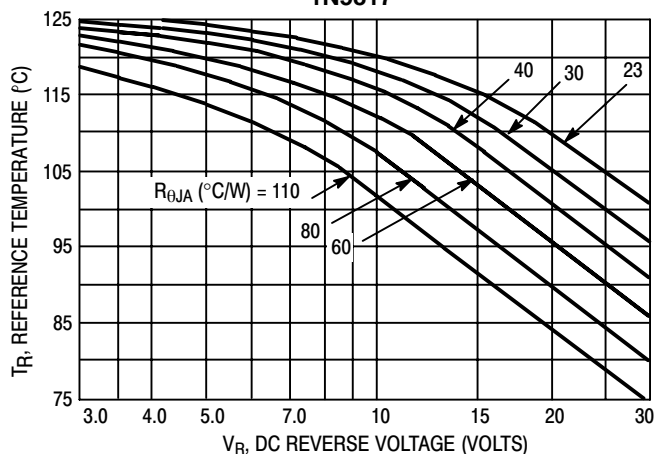


Figure 2. Maximum Reference Temperature 1N5818

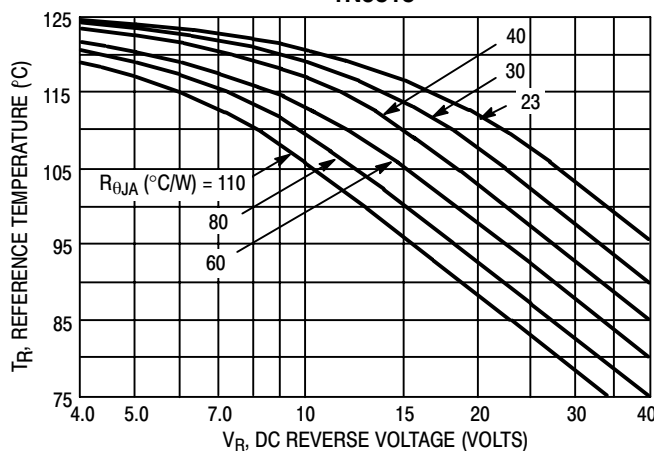


Figure 3. Maximum Reference Temperature 1N5819

Table 1. Values for Factor F

Circuit	Half Wave		Full Wave, Bridge		Full Wave, Center Tapped* †	
	Resistive	Capacitive*	Resistive	Capacitive	Resistive	Capacitive
Sine Wave	0.5	1.3	0.5	0.65	1.0	1.3
Square Wave	0.75	1.5	0.75	0.75	1.5	1.5

\*\*Note that  $V_{R(PK)} \approx 2.0 V_{in(PK)}$ .

†Use line to center tap voltage for  $V_{in}$ .

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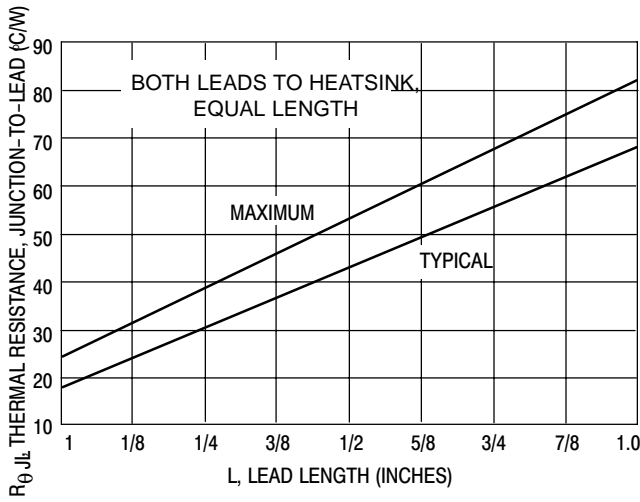


Figure 4. Steady-State Thermal Resistance

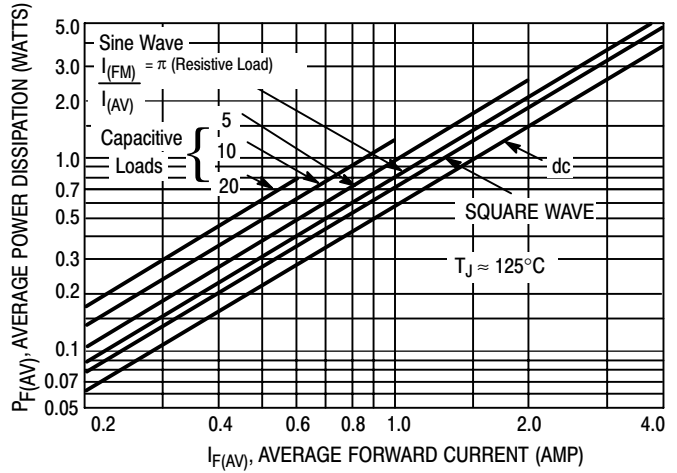


Figure 5. Forward Power Dissipation  
1N5817-19

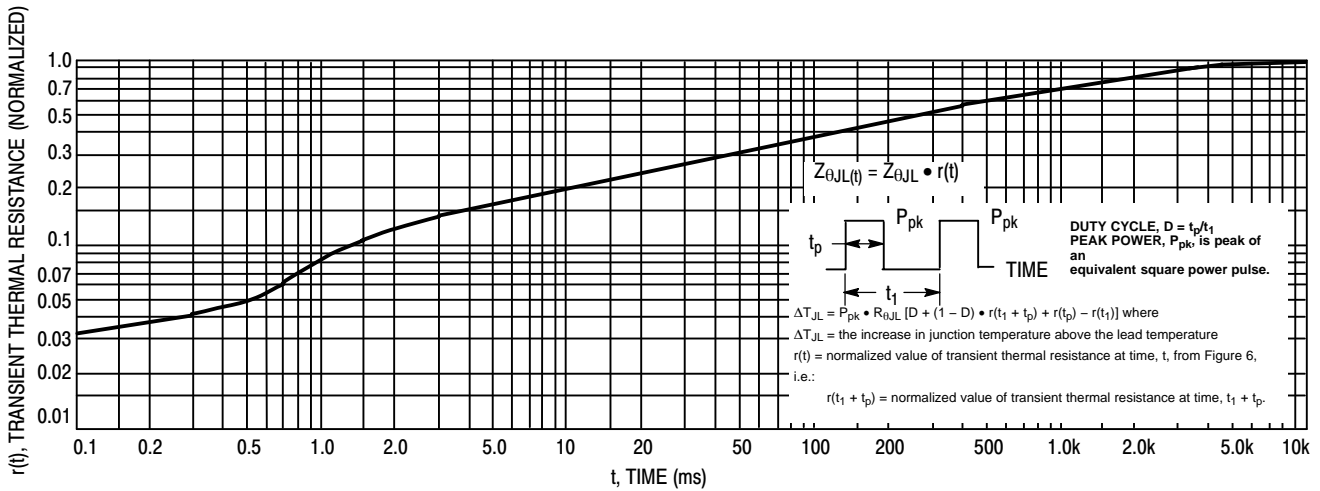


Figure 6. Thermal Response

### NOTE 4. — MOUNTING DATA

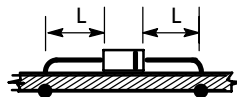
Data shown for thermal resistance, junction-to-ambient ( $R_{\theta_{JA}}$ ) for the mountings shown is to be used as typical guideline values for preliminary engineering, or in case the tie point temperature cannot be measured.

### TYPICAL VALUES FOR $R_{\theta_{JA}}$ IN STILL AIR

Mounting Method	Lead Length, L (in)				$R_{\theta_{JA}}$
	1/8	1/4	1/2	3/4	
1	52	65	72	85	$^{\circ}\text{C}/\text{W}$
2	67	80	87	100	$^{\circ}\text{C}/\text{W}$
3	50				$^{\circ}\text{C}/\text{W}$

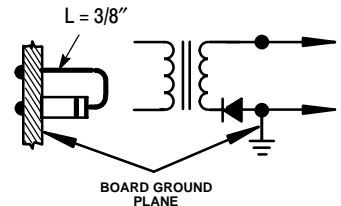
#### Mounting Method 1

P.C. Board with 1-1/2" x 1-1/2" copper surface.

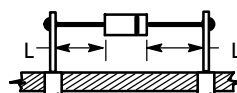


#### Mounting Method 3

P.C. Board with 1-1/2" x 1-1/2" copper surface.



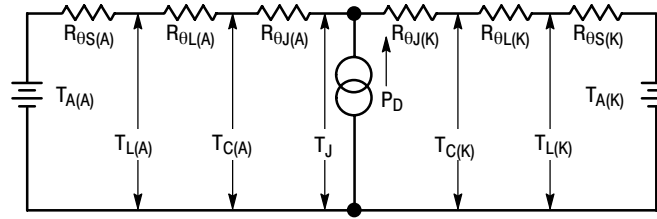
#### Mounting Method 2



VECTOR PIN MOUNTING

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## NOTE 5. — THERMAL CIRCUIT MODEL (For heat conduction through the leads)



Use of the above model permits junction to lead thermal resistance for any mounting configuration to be found. For a given total lead length, lowest values occur when one side of the rectifier is brought as close as possible to the heatsink. Terms in the model signify:

- $T_A$  = Ambient Temperature       $T_C$  = Case Temperature
- $T_L$  = Lead Temperature           $T_J$  = Junction Temperature
- $R_{\theta S}$  = Thermal Resistance, Heatsink to Ambient
- $R_{\theta L}$  = Thermal Resistance, Lead to Heatsink
- $R_{\theta J}$  = Thermal Resistance, Junction to Case
- $P_D$  = Power Dissipation

(Subscripts A and K refer to anode and cathode sides, respectively.) Values for thermal resistance components are:

- $R_{\theta L} = 100^\circ\text{C/W/in}$  typically and  $120^\circ\text{C/W/in}$  maximum
- $R_{\theta J} = 36^\circ\text{C/W}$  typically and  $46^\circ\text{C/W}$  maximum.

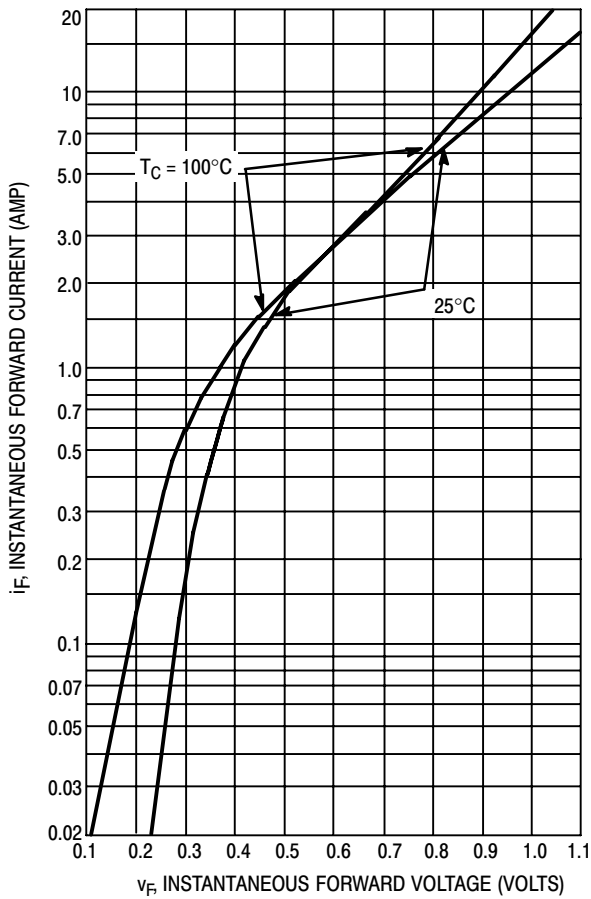


Figure 7. Typical Forward Voltage

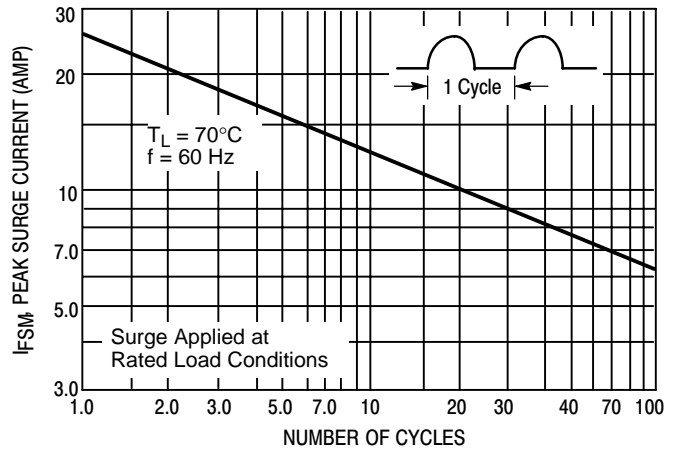


Figure 8. Maximum Non-Repetitive Surge Current

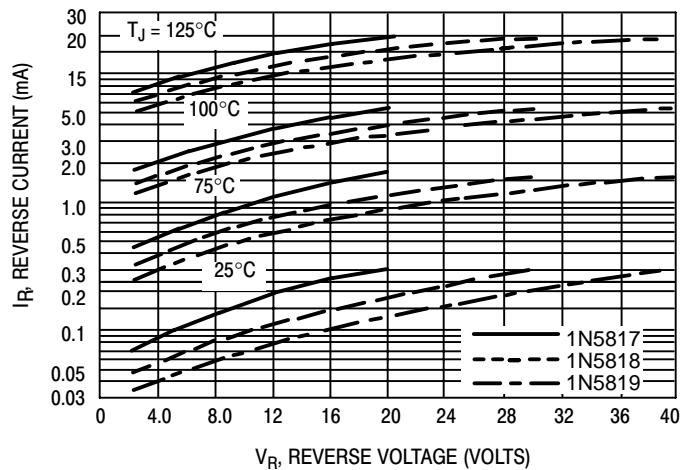


Figure 9. Typical Reverse Current

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## NOTE 6. — HIGH FREQUENCY OPERATION

Since current flow in a Schottky rectifier is the result of majority carrier conduction, it is not subject to junction diode forward and reverse recovery transients due to minority carrier injection and stored charge. Satisfactory circuit analysis work may be performed by using a model consisting of an ideal diode in parallel with a variable capacitance. (See Figure 10.)

Rectification efficiency measurements show that operation will be satisfactory up to several megahertz. For example, relative waveform rectification efficiency is approximately 70 percent at 2.0 MHz, e.g., the ratio of dc power to RMS power in the load is 0.28 at this frequency, whereas perfect rectification would yield 0.406 for sine wave inputs. However, in contrast to ordinary junction diodes, the loss in waveform efficiency is not indicative of power loss: it is simply a result of reverse current flow through the diode capacitance, which lowers the dc output voltage.

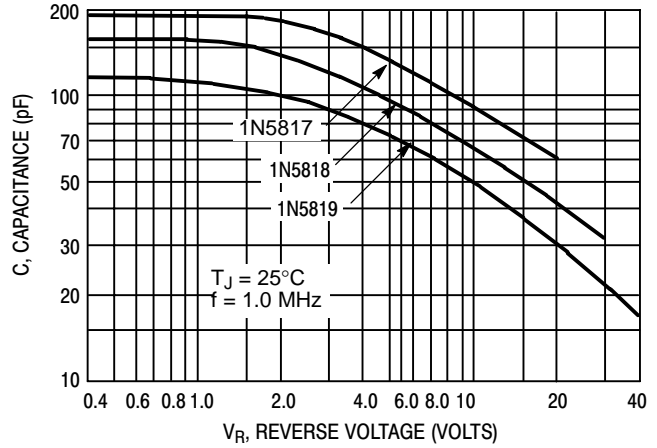


Figure 10. Typical Capacitance

## ORDERING INFORMATION

Device	Package	Shipping†
1N5817	Axial Lead*	1000 Units / Bag
1N5817G	Axial Lead*	1000 Units / Bag
1N5817RL	Axial Lead*	5000 / Tape & Reel
1N5817RLG	Axial Lead*	5000 / Tape & Reel
1N5818	Axial Lead*	1000 Units / Bag
1N5818G	Axial Lead*	1000 Units / Bag
1N5818RL	Axial Lead*	5000 / Tape & Reel
1N5818RLG	Axial Lead*	5000 / Tape & Reel
1N5819	Axial Lead*	1000 Units / Bag
1N5819G	Axial Lead*	1000 Units / Bag
1N5819RL	Axial Lead*	5000 / Tape & Reel
1N5819RLG	Axial Lead*	5000 / Tape & Reel

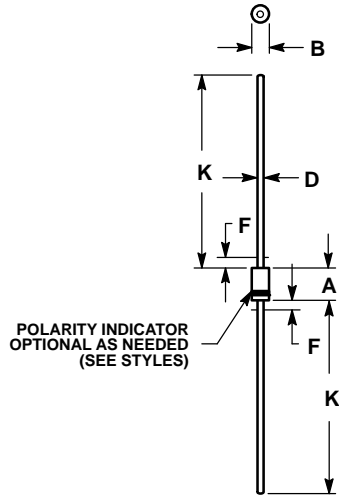
†For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specifications Brochure, BRD8011/D.

\*This package is inherently Pb-Free.

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## PACKAGE DIMENSIONS

### AXIAL LEAD CASE 59-10 ISSUE U




#### NOTES:

1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
2. CONTROLLING DIMENSION: INCH.
3. ALL RULES AND NOTES ASSOCIATED WITH JEDEC DO-41 OUTLINE SHALL APPLY
4. POLARITY DENOTED BY CATHODE BAND.
5. LEAD DIAMETER NOT CONTROLLED WITHIN F DIMENSION.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.161	0.205	4.10	5.20
B	0.079	0.106	2.00	2.70
D	0.028	0.034	0.71	0.86
F	----	0.050	----	1.27
K	1.000	----	25.40	----

#### STYLE 1:

1. CATHODE (POLARITY BAND)
2. ANODE

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- Подбор аналогов.
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- Работу по проектам и поставку образцов.
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- Тестирование поставляемой продукции.
- Поставку компонентов, требующих военную и космическую приемку.
- Входной контроль качества.
- Наличие сертификата ISO.

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- Регистрацию проекта у производителя компонентов.
- Техническую поддержку проекта.
- Защиту от снятия компонента с производства.
- Оценку стоимости проекта по компонентам.
- Изготовление тестовой платы монтаж и пусконаладочные работы.



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