

### DESCRIPTION

The MP155 is a primary-side regulator that provides accurate constant voltage regulation without the opto-coupler, and supports Buck, Buck-boost, Boost and Flyback topologies. An integrated 500V MOSFET simplifies the structure and reduces costs. These features make it a competitive candidate for off-line low-power applications, such as home appliances and standby power.

The MP155 is a green-mode-operation regulator. Both the peak current and the switching frequency decrease as the load decreases. As a result, it offers excellent efficiency performance at light load, thus improving the overall average efficiency.

The MP155 features various protections such as thermal shutdown (TSD), VCC under-voltage lockout (UVLO), overload protection (OLP), short-circuit protection (SCP), and open loop protection.

The MP155 is available in the TSOT23-5 and SOIC8 packages.

### FEATURES

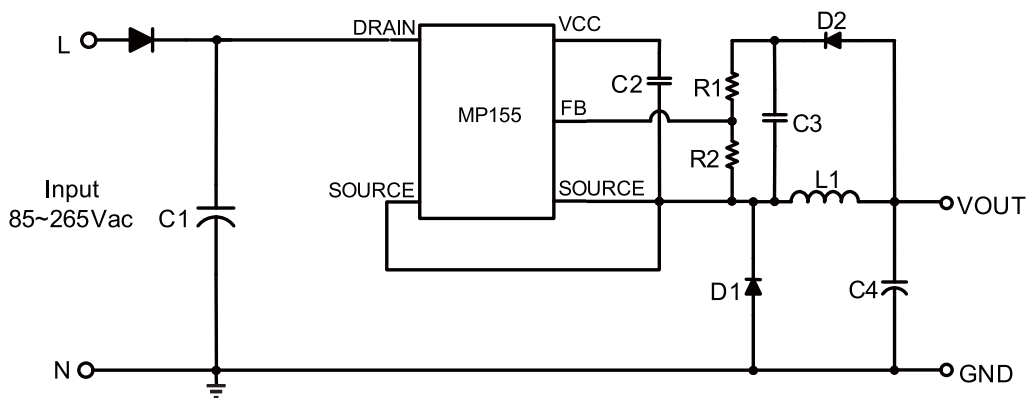
- Primary-side constant voltage (CV) control, supporting Buck, Buck-boost, Boost and Flyback topologies
- Integrated 500V/20Ω MOSFET
- < 100mW No-load power consumption
- Up to 4W output power
- Maximum DCM output current of 130mA
- Maximum CCM output current of 220mA
- Low VCC operating current
- Frequency foldback
- Maximum frequency limit
- Peak current compression
- Internal high-voltage current source
- Internal 350ns leading-edge blanking
- Thermal shutdown (auto restart)
- VCC under-voltage lockout with hysteresis (UVLO)
- Timer-based overload protection.
- Short circuit protection
- Open loop protection

### APPLICATIONS

- Home Appliances, white goods and consumer electronics
- Industrial Controls
- Standby Power

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### TYPICAL APPLICATION



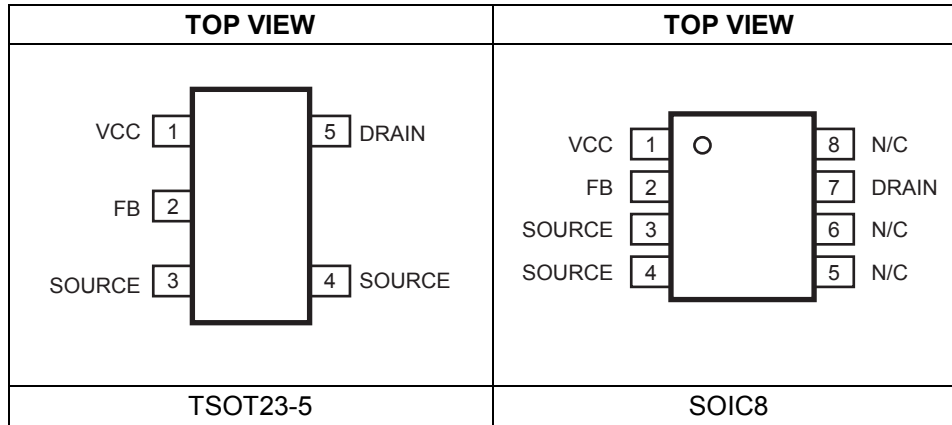
### ORDERING INFORMATION

Part Number*	Package	Top Marking
MP155GJ	TSOT23-5	AEN
MP155GS	SOIC8	MP155

\* For Tape & Reel, add suffix -Z (e.g. MP155GJ-Z);

\* For Tape & Reel, add suffix -Z (e.g. MP155GS-Z);

### PACKAGE REFERENCE



#### ABSOLUTE MAXIMUM RATINGS <sup>(1)</sup>

Drain to SOURCE .....	-0.7V to 500V
All the other Pin .....	-0.7V to 6.5V
Continuous Power Dissipation (T <sub>A</sub> = +25°C) <sup>(2)</sup>	
TSOT23-5.....	1W
SOIC8.....	1W
Junction Temperature.....	150°C
Lead Temperature .....	260°C
Storage Temperature.....	-60°C to +150°C
ESD Capability Human Body Mode .....	4.0kV
ESD Capability Machine Mode .....	200V

#### Recommended Operating Conditions <sup>(3)</sup>

Operating Junction Temp. (T <sub>J</sub> ).	-40°C to +125°C
Operating VCC range .....	5.3V to 5.6V

#### Thermal Resistance <sup>(4)</sup>

	$\theta_{JA}$	$\theta_{JC}$
TSOT23-5 .....	100 .....	55 ... °C/W
SOIC8 .....	96 .....	45 ... °C/W

#### Notes:

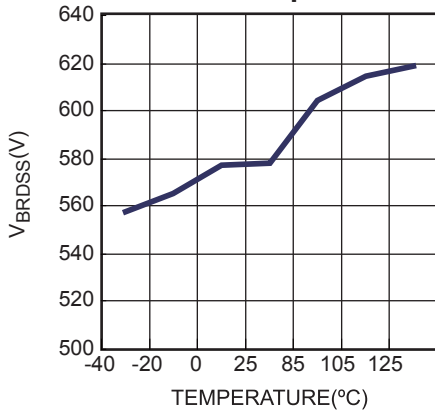
- Exceeding these ratings may damage the device.
- The maximum allowable power dissipation is a function of the maximum junction temperature T<sub>J</sub>(MAX), the junction-to-ambient thermal resistance  $\theta_{JA}$ , and the ambient temperature T<sub>A</sub>. The maximum allowance continuous power dissipation at any ambient temperature is calculated by PD(MAX)=(T<sub>J</sub>(MAX)-T<sub>A</sub>)/ $\theta_{JA}$ . Exceeding the maximum allowance power dissipation will cause excessive die temperature, and the regulator will go into thermal shutdown. Internal thermal shutdown circuit protects the device from permanent damage.
- The device is not guaranteed to function outside of its operating conditions.
- Measured on JESD51-7, 4-layer PCB.

**ELECTRICAL CHARACTERISTICS**
**V<sub>CC</sub> = 5.8V, T<sub>A</sub> = 25°C, unless otherwise noted.**

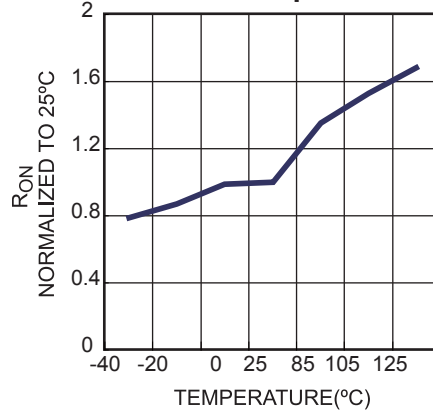
Parameter	Symbol	Condition	Min	Typ	Max	Units
<b>Start-up Current Source (Drain Pin)</b>						
Internal regulator supply current	I <sub>regulator</sub>	V <sub>CC</sub> =4V; V <sub>Drain</sub> =100V	2.5	3.5	4.5	mA
Drain pin leakage current	I <sub>Leak</sub>	V <sub>CC</sub> =5.8V; V <sub>Drain</sub> =400V		10	12	μA
Breakdown Voltage	V <sub>(BR)DSS</sub>		500			V
<b>Supply Voltage Management (VCC Pin)</b>						
VCC regulator turn-off level (rising)	V <sub>CCOFF</sub>		5.4	5.6	5.8	V
VCC regulator turn-on level (falling)	V <sub>CCON</sub>		5.1	5.3	5.6	V
On and off VCC regulator hysteresis				250		mV
VCC turn-off level (falling)	V <sub>CCstop</sub>			3.4		V
VCC phase completion level (falling)	V <sub>CCpro</sub>			2.4		V
Internal IC consumption	I <sub>CC</sub>	V <sub>CC</sub> =5.8V, f <sub>s</sub> =37kHz, D=40%			430	μA
Internal IC consumption (no switching)	I <sub>CC</sub>				250	μA
Internal IC Consumption, latch-off phase	I <sub>CCLATCH</sub>	V <sub>CC</sub> =5.3V		16		μA
<b>Internal MOSFET (Drain Pin)</b>						
Breakdown voltage	V <sub>BRDSS</sub>		500			V
ON-State resistance	R <sub>on</sub>			20		Ω
<b>Internal Current Sense</b>						
Peak current limit	I <sub>Limit</sub>		260	290	345	mA
Leading-edge blanking	τ <sub>LEB1</sub>			350		ns
SCP point	I <sub>SCP</sub>			450		mA
Leading-edge blanking for SCP	τ <sub>LEB2</sub>			180		ns
<b>Feedback input (FB Pin)</b>						
Minimum OFF time	τ <sub>minoff</sub>		15	18	21	μs
Primary MOSFET feedback turn-on threshold	V <sub>FB</sub>		2.4	2.5	2.6	V
OLP feedback trigger threshold	V <sub>FB OLP</sub>		1.6	1.7	1.8	V
Over-load protection delay	τ <sub>OLP</sub>	f <sub>s</sub> =37kHz		170		ms
Open loop detection	V <sub>OLD</sub>			60		mV
<b>Thermal Shutdown</b>						
Thermal shutdown threshold				150		°C

### TYPICAL CHARACTERISTICS

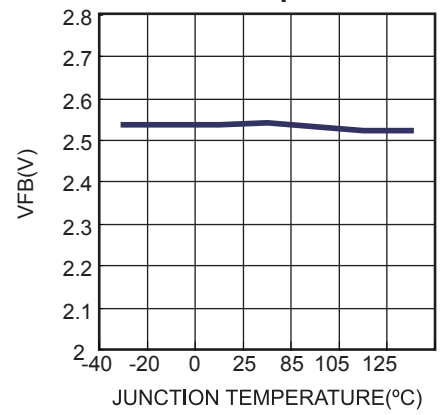
**Breakdown Voltage vs. Junction Temperature**



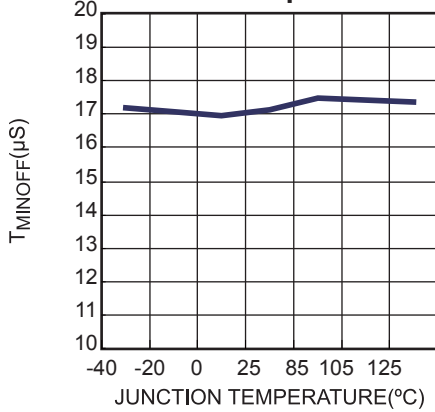
**On-State Resistance vs. Junction Temperature**



**Feedback Voltage vs. Junction Temperature**

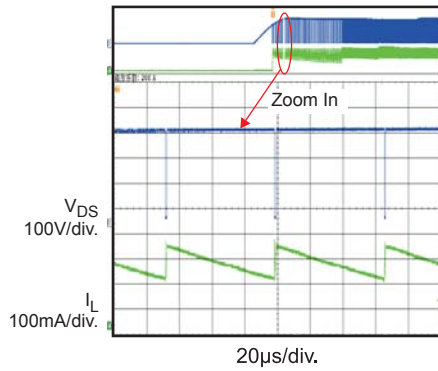
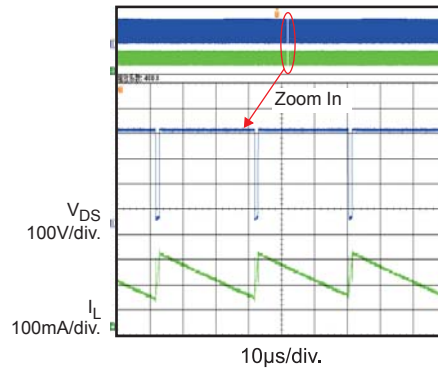
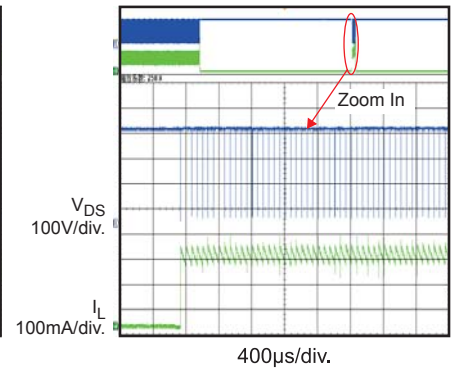
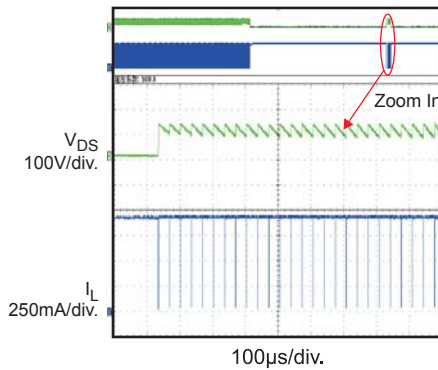


**Minimum Off Time vs. Junction Temperature**



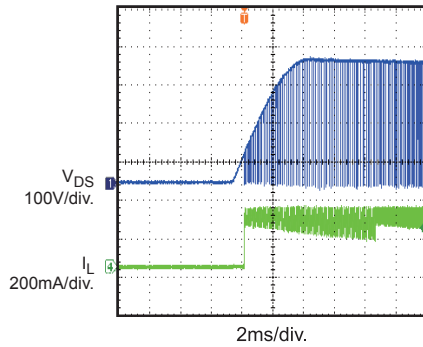
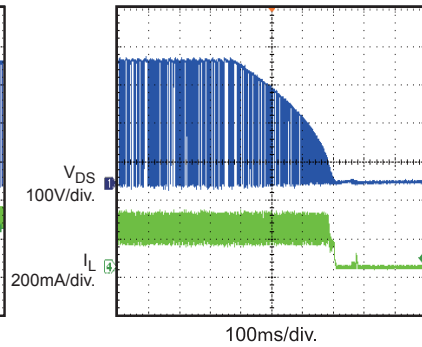
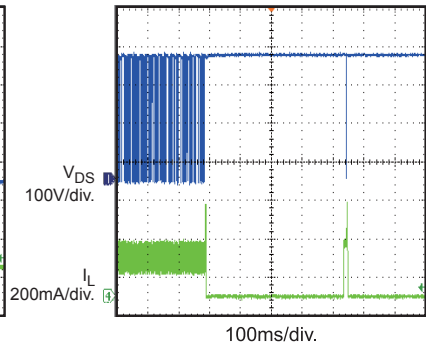
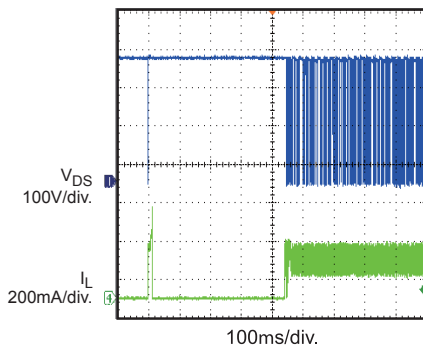
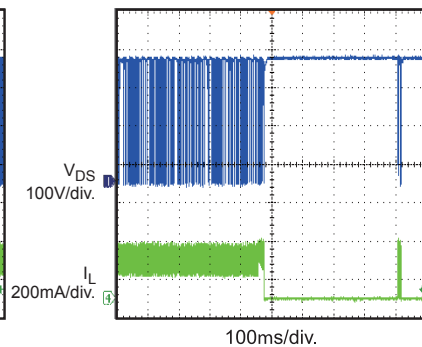
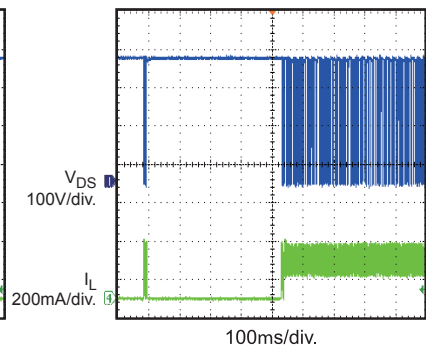
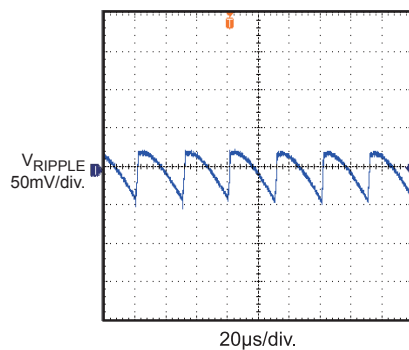
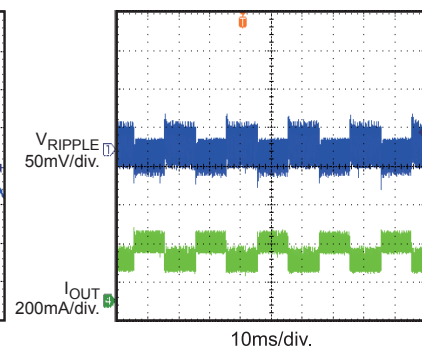
## TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN} = 265VAC$ ,  $V_{OUT} = 12V$ ,  $I_{OUT} = 200mA$ ,  $L = 2.2mH$ ,  $C_{OUT} = 100\mu F$ ,  $T_A = +25^{\circ}C$ , unless otherwise noted.

**Start up**

**Normal operation**

**SCP**

**Open Loop Protection**


**TYPICAL PERFORMANCE CHARACTERISTICS (continued)**

$V_{IN} = 230VAC$ ,  $V_{OUT} = 12V$ ,  $I_{OUT} = 200mA$ ,  $L = 2.2mH$ ,  $C_{OUT} = 100\mu F$ ,  $T_A = +25^\circ C$ , unless otherwise noted.

**Input Power Start Up**

**Input Power Shut Down**

**SCP Entry**

**SCP recovery**

**Open Loop Entry**

**Open Loop Recovery**

**Output Voltage Ripple**

**Load Transient**


**PIN FUNCTIONS**

Pin # TSOT23-5	Pin # SOIC8	Name	Description
1	1	VCC	Control Circuit Power Supply.
2	2	FB	Regulator Feedback.
3,4	3,4	SOURCE	Internal Power MOSFET Source. Ground reference for VCC and FB pins.
5	7	DRAIN	Internal Power MOSFET Drain. High-voltage current source input.
	5,6,8	N/C	Not connected.

FUNCTIONAL BLOCK DIAGRAM

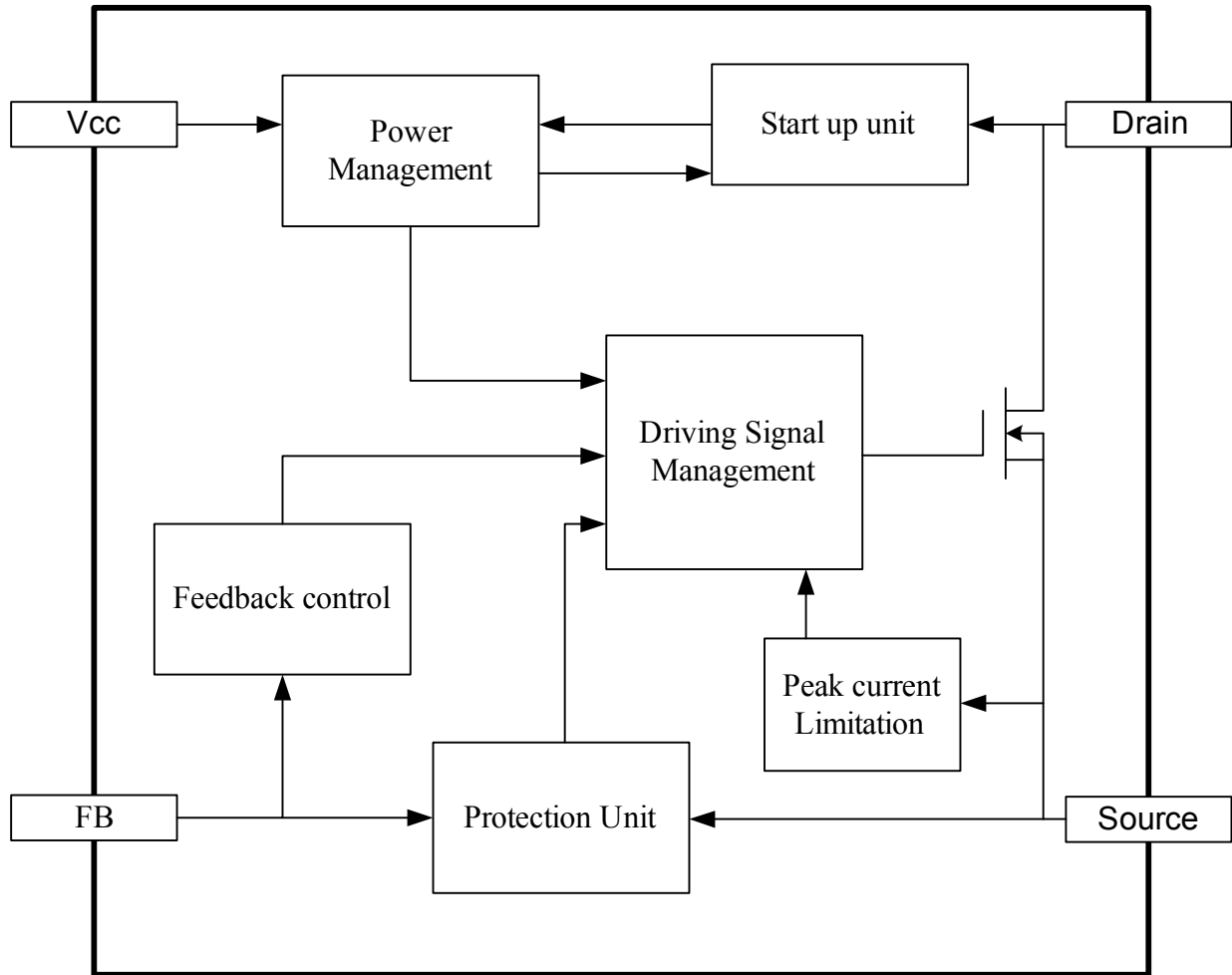


Figure 1: Functional Block Diagram



## OPERATION

The MP155 is a green-mode-operation regulator. The peak current and the switching frequency both decrease as the load decreases to provide excellent efficiency at light load, and thus improve the overall average efficiency. The typical application diagram shows that the regulator operates using a minimal number of external components. It incorporates the following features:

### Start-up and Under Voltage Lock-out

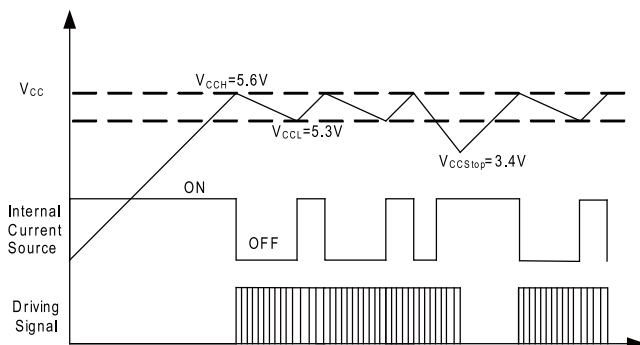
The internal high-voltage regulator supplies IC from the Drain pin. The IC starts switching and the internal high voltage regulator turns off when the voltage on VCC reaches 5.6V. When the VCC voltage drops below 5.3V, the internal high voltage regulator turns on again to charge the external VCC capacitor. Use a capacitor in the several  $\mu\text{F}$  range stabilize the VCC voltage and this can lower the cost by decreasing the value of the capacitor.

When the voltage on VCC drops below 3.4V, the IC stops, then the internal high-voltage regulator charges the VCC capacitor.

When faults occur, such as overload, short circuit, and over-heating, the IC stops working and an internal current source (16 $\mu\text{A}$ ) discharges the VCC capacitor. Before the VCC voltage drops below 2.4V, the internal high-voltage regulator remains off and the VCC capacitor remains discharged. Estimate the restart time after a fault as:

$$\tau_{\text{restart}} = C_{\text{VCC}} \times \frac{V_{\text{CC}} - 2.4\text{V}}{16\mu\text{A}} + C_{\text{VCC}} \times \frac{5.6\text{V} - 2.4\text{V}}{3.5\text{mA}}$$

Figure 2 shows the typical waveform with VCC under voltage lock out.



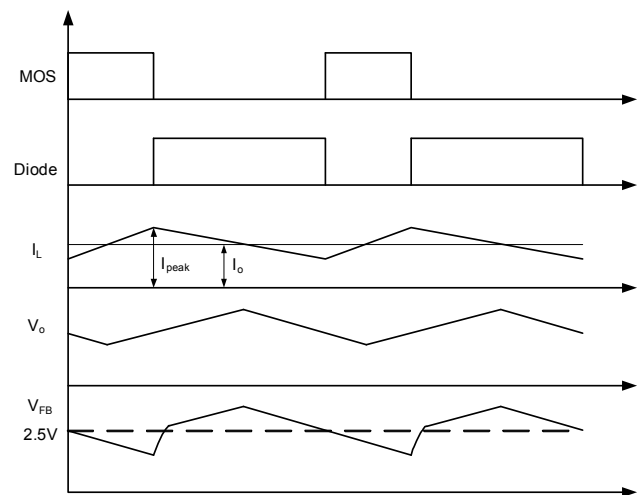
**Figure 2: VCC Under-Voltage Lockout**

### Constant Voltage Operation

The MP155 is a fully-integrated regulator when used in a Buck solution as shown in the typical application on page 1.

The integrated MOSFET turns ON at the beginning of each cycle when the feedback voltage is below the reference voltage (2.5V), which indicates insufficient output voltage. The peak current limit determines the ON period. After the ON period elapses, the integrated MOSFET turns OFF. The freewheeling diode (D1) remains OFF until the inductor current charges the sampling capacitor (C3) voltage to the output voltage level. Then the sampling capacitor voltage changes with the output voltage. The sampling capacitor can sample and hold the output voltage to regulate the output voltage. The sampling capacitor voltage decreases after the inductor current drops below the output current. When the feedback voltage falls below the reference voltage (2.5V), a new switching cycle begins.

Figure 3 shows the detailed operation timing diagram under CCM.



**Figure 3:  $V_{\text{FB}}$  vs.  $V_{\text{out}}$**

Monitoring the sampling capacitor regulates the output voltage can be regulated, as per the following equation:

$$V_o = 2.5\text{V} \times \frac{R1 + R2}{R2}$$

**Frequency Foldback**

Under light load or no load conditions, the output drops very slowly, which increases the time for the MOSFET to turn ON again; i.e., frequency decreases as the load decreases. So the MP155 can maintain a high efficiency under light load condition by reducing the switching frequency automatically.

The switching frequency can be obtained as:

$$f_s = \frac{(V_{in} - V_o)}{2L(I_{peak} - I_o)} \cdot \frac{V_o}{V_{in}}, \text{ for CCM}$$

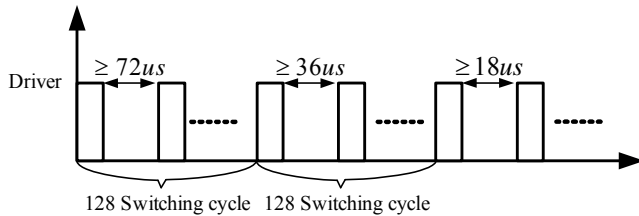
$$f_s = \frac{2(V_{in} - V_o)}{LI_{peak}^2} \cdot \frac{I_o V_o}{V_{in}}, \text{ for DCM}$$

At the same time, the peak current limit decreases from 290mA as the OFF time increases. In standby mode, the frequency and the peak current are both minimized, allowing for a small dummy load. As a result, the peak-current-compression function helps to reduce no-load consumption. Determine the peak current limitation from the following equation where  $\tau_{off}$  is the power module OFF time:

$$I_{Peak} = 290\text{mA} - (1\text{mA}/\mu\text{S}) \times (\tau_{off} - 18\mu\text{S})$$

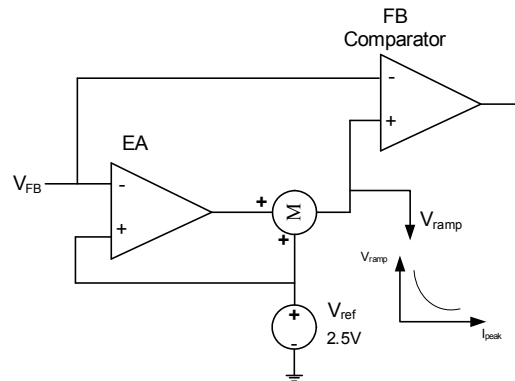
**Minimum off time limitation**

The MP155 implements a minimum OFF time limit. During the normal operation, the minimum OFF time limit is 18 $\mu\text{s}$ ; during start up, the minimum OFF time limit gradually drops from 72 $\mu\text{s}$ , to 36 $\mu\text{s}$ , then to 18  $\mu\text{s}$  (see Figure 4). Each minimum OFF time has 128 switching cycles. This soft-start function allows for safe start-up.



**Figure 4:  $\tau_{minoff}$  at Start-Up**

**EA Compensation**



**Figure 5: EA and Ramp Compensation**

To improve load regulation, the MP155 implements an error amplifier (EA) compensation function ( Figure 5 ). The MP155 samples the feedback voltage 6 $\mu\text{s}$  after the MOSFET turns off. EA compensation regulates the 2.5V reference voltage with the load, thus improving the power module regulation.

**RAMP Compensation**

An internal ramp compensation circuit precisely maintains the output voltage. An additional exponential voltage sinking source pulls down the feedback comparator's reference voltage as shown in Figure 5. The ramp compensation is relative to the load conditions: Under full-load conditions, the compensation is  $\sim 1\text{mV}/\mu\text{s}$ ; with a decreasing load, the compensation increases exponentially.

**Over Load Protection (OLP)**

As the load increases, the peak current and the switching frequency increase with the load. When the switching frequency and peak current reaches their maximums, the output voltage will decrease if the load continues to increase. Then the FB voltage will drop below OLP threshold.

By continuously monitoring the FB voltage, the timer starts when the FB voltage drops below the 1.7V error flag threshold. Removing the error flag resets the timer. If the timer continues to completion at 170ms ( $f_s = 37\text{kHz}$ ), OLP occurs. This timer duration avoids triggering OLP when the power supply starts up or enters a load transition phase, and therefore requires that the power supply start up in less than 170ms. A different switching frequency ( $f_s$ ) changes the over-load protection delay time, as shown below:

$$\tau_{\text{Dealy}} \approx 170\text{ms} \times \frac{37\text{kHz}}{f_s}$$

### Short Circuit Protection (SCP)

The MP155 shuts down when the peak current rises above 450mA as its short-circuit protection threshold. The power supply resumes operation after removing the fault.

### Thermal shutdown (TSD)

To prevent from any lethal thermal damage, the MP155 shuts down switching when the inner temperature exceeds 150°C. During thermal shutdown (TSD), the VCC drops to 2.4V, and then the internal high voltage regulator recharges VCC.

### Open Loop Detection

If the  $V_{\text{FB}}$  drops below 60mV, the IC will stop working and begins a re-start cycle. The open-loop detection is blanked for 128 switching cycles during start-up.

### Leading-Edge Blanking

An internal leading-edge blanking (LEB) unit between the current sense resistor inside the IC and the current comparator input avoids prematurely switching pulse termination due to the parasitic capacitance. During the blanking period, the current comparator is disabled and cannot turn off the external MOSFET. Figure 6 shows leading-edge blanking.

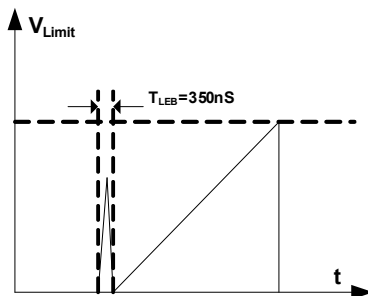


Figure 6: Leading-Edge Blanking

**APPLICATION INFORMATION**
**Table 1. Common Topologies Using MP155**

Topology	Circuit Schematic	Features
<b>High-Side Buck</b>		<ol style="list-style-type: none"> <li>1. <b>No-isolation,</b></li> <li>2. <b>Positive output</b></li> <li>3. <b>Low cost</b></li> <li>4. <b>Direct feedback</b></li> </ol>
<b>High-Side Buck-Boost</b>		<ol style="list-style-type: none"> <li>1. <b>No-isolation,</b></li> <li>2. <b>Negative output</b></li> <li>3. <b>Low cost</b></li> <li>4. <b>Direct feedback</b></li> </ol>
<b>Boost</b>		<ol style="list-style-type: none"> <li>1. <b>No-isolation,</b></li> <li>2. <b>Positive output</b></li> <li>3. <b>Low cost</b></li> <li>4. <b>Direct feedback</b></li> </ol>
<b>Flyback</b>		<ol style="list-style-type: none"> <li>1. <b>Isolation,</b></li> <li>2. <b>Positive output</b></li> <li>3. <b>Low cost</b></li> <li>4. <b>Indirect feedback</b></li> </ol>

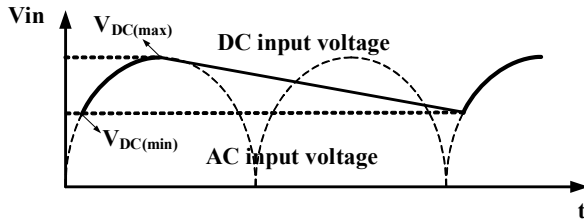
**Topology Options**

MP155 can be used in common topologies, such as Buck, Buck-Boost, Boost and Flyback. Please find the Table.1 for more information.

**Component Selection**

**Input Capacitor**

The input capacitor supplies the converter’s DC input voltage. Figure 7 shows the typical half-wave rectifier’s DC bus voltage waveform.



**Figure 7: Input Voltage Waveform**

When using the half-wave rectifier, set the input capacitor 3µF/W for the universal input condition. When using the full-wave rectifier, choose a smaller capacitor, but avoid a minimum DC voltage below 70V to avoid thermal shutdown.

**Inductor**

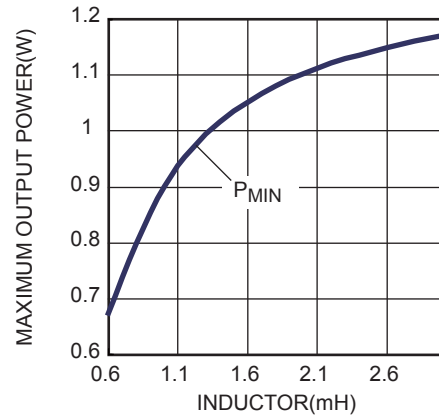
MP155 has a minimum off time limit that determines the maximum power output. The maximum power increases with the inductor value. Using a smaller inductor may cause the output to fail at full load, but a larger inductor results in a higher OLP load. The optimal inductor value is the smallest that can supply the rated power. The maximum power is:

$$P_{o\max} = V_o \left( I_{\text{peak}} - \frac{V_o \tau_{\text{minoff}}}{2L} \right), \text{ for CCM}$$

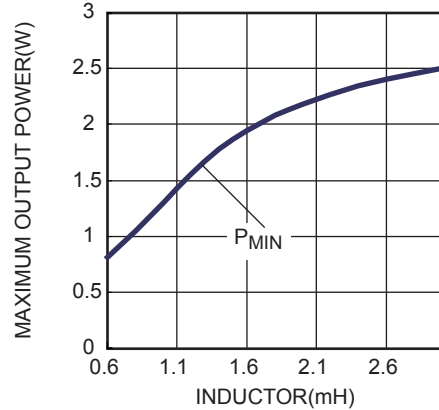
$$P_{o\max} = \frac{1}{2} L I_{\text{peak}}^2 \cdot \frac{1}{\tau_{\text{minoff}}}, \text{ for DCM}$$

To account for converter parameters—such as peak current limit and minimum OFF time—estimate the minimum inductor power ( $P_{\text{min}}$ ) for the maximum power, and selecting an inductor with a  $P_{\text{min}}$  value that exceeds the rated power.

Using output voltages 5V and 12V as examples, Figure 8 shows the curve for  $P_{\text{min}}$  at 5V, and Figure 9 shows the curve for  $P_{\text{min}}$  at 12V. ( $I_{\text{peak}}=0.29\text{A}$ ,  $\tau_{\text{minoff}}=18\mu\text{s}$ )



**Figure 8:  $P_{\text{min}}$  vs. L for 5V**



**Figure 9:  $P_{\text{min}}$  vs. L for 12V**

When designing a 0.5W converter (5V, 0.1A), estimate the minimum inductor value at 0.6mH based on Figure 8. Similarly, for a 1.2W converter (12V, 0.1A), estimate the minimum inductor at 0.9mH based on Figure 9 .

Use a standard off-the-shelf inductor to reduce costs. Use a standard inductance that exceeds calculated inductance.

**Freewheeling Diode**

Choose a diode with a maximum reverse voltage rating that exceeds the maximum input voltage, and a current rating that exceeds the output current.

The reverse recovery of the freewheeling diode can affect the efficiency and circuit operation. Select an ultra-fast diode, such as the EGC10JH.

### Output Capacitor

The output capacitor maintains the DC output voltage. Estimate the output voltage ripple as:

$$V_{CCM\_ripple} = \frac{\Delta i}{8f_s C_o} + \Delta i \cdot R_{ESR}, \text{ for CCM}$$

$$V_{DCM\_ripple} = \frac{I_o}{f_s C_o} \cdot \left( \frac{I_{pk} - I_o}{I_{pk}} \right)^2 + I_{pk} \cdot R_{ESR}, \text{ for DCM}$$

Use ceramic, tantalum, or low-ESR electrolytic capacitors to lower the output voltage ripple.

### Feedback Resistors

The resistor divider determines the output voltage. Choose appropriate R1 and R2 values to maintain the FB voltage at 2.5V. Avoid very large values for R2 (typical values between 5kΩ to 10kΩ).

### Feedback Capacitor

The feedback capacitor provides a sample-and-hold function. Small capacitors result in poor regulation at light load condition, and large capacitors can impact circuit operation. Estimate the capacitor range as per the following equation:

$$\frac{1}{2} \frac{V_o}{R_1 + R_2} \cdot \frac{C_o}{I_o} \leq C_{FB} \leq \frac{V_o}{R_1 + R_2} \cdot \frac{C_o}{I_o}$$

Choose an appropriate value given practical considerations.

### Dummy Load

A dummy load maintains the load regulation. This ensures sufficient inductor energy to charge the sample-and-hold capacitor to detect the output voltage. Start with a 3mA dummy load and adjust as necessary.

### VCC Supply

The MP155 obtains a low no-load power consumption by external VCC supply. This supply is dependent on the value of  $V_{out}$ . Connect a diode and resistor between C2 and C3 as per the values listed in Table 2.

**Table 2: Recommended VCC Supply Resistor Values**

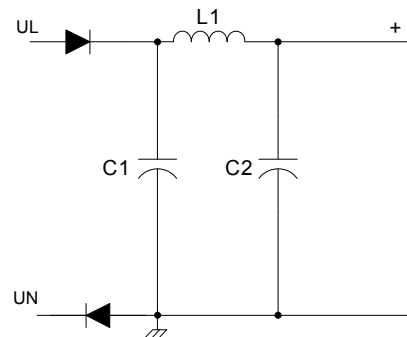
V <sub>OUT</sub>	Resistor value
3.3V	NC <sup>(5)</sup>
5V	NC
12V	24.8k
16V	40.8k
24V	72.8k

**Notes:**

5) NC= no connection.

### Surge Performance

To obtain a good surge performance, select an appropriate input capacitor that meets different surge tests. Figure 10 shows the half-wave rectifier. Table 3 shows the required capacitance under normal conditions for different surge voltages.



**Figure 10: Half-Wave Rectifier**

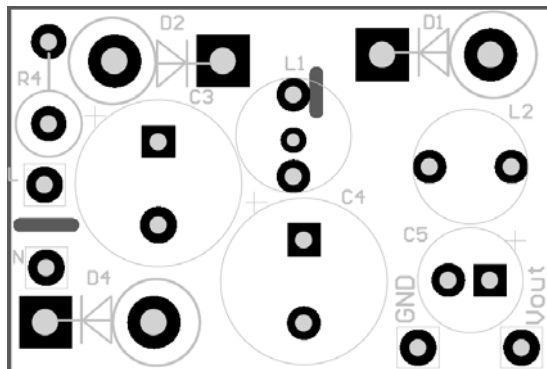
**Table 3: Recommended Capacitor Values**

Surge voltage	500V	1000V	2000V
<b>C1</b>	1μF	10μF	22μF
<b>C2</b>	1μF	4.7μF	10μF

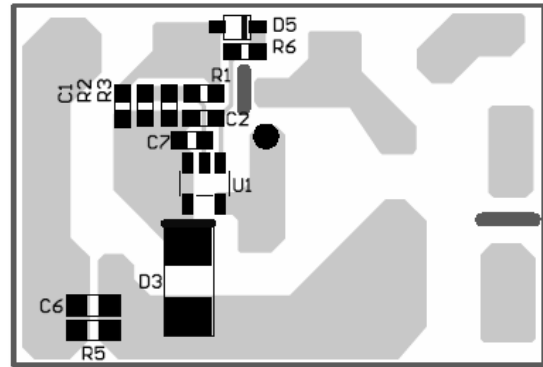
### Layout Guide

PCB layout is very important to achieve reliable operation, and good EMI and thermal performance. Follow these guidelines to optimize performance.

- 1) Minimize the loop area formed by the input capacitor, IC part, freewheeling diode, inductor and output capacitor.
- 2) Place the power inductor far away from the input filter.
- 3) Add a capacitor in the several-hundred pF range between pin FB and source as close to the IC as possible.
- 4) Connect the exposed pad with the Drain pin to a large copper area to improve thermal performance.



**Top**



**Bottom Layer**

### Design Example

Below is a design example following the application guidelines given the following specifications:

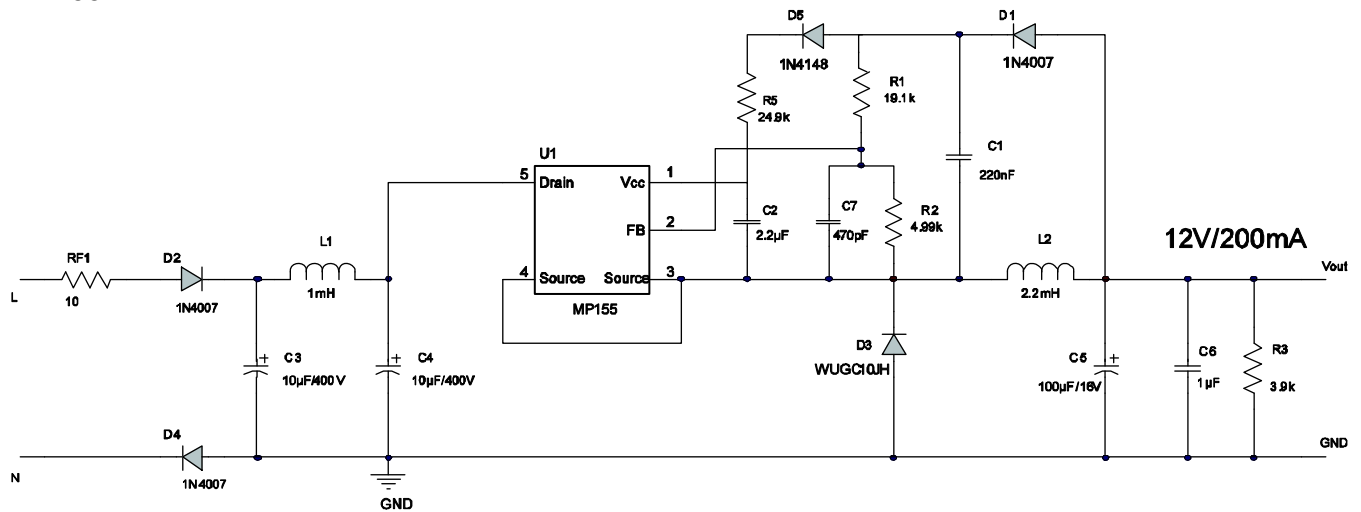
**Table 4: Design Example**

$V_{IN}$	85 to 265Vac
$V_{OUT}$	12V
$I_{OUT}$	200mA

Figure 11 shows the detailed application schematic. The Typical Performance Characteristics section lists typical performance and circuit waveforms. For more device application, please refer to the related Evaluation Board Datasheets.

## TYPICAL APPLICATION CIRCUITS

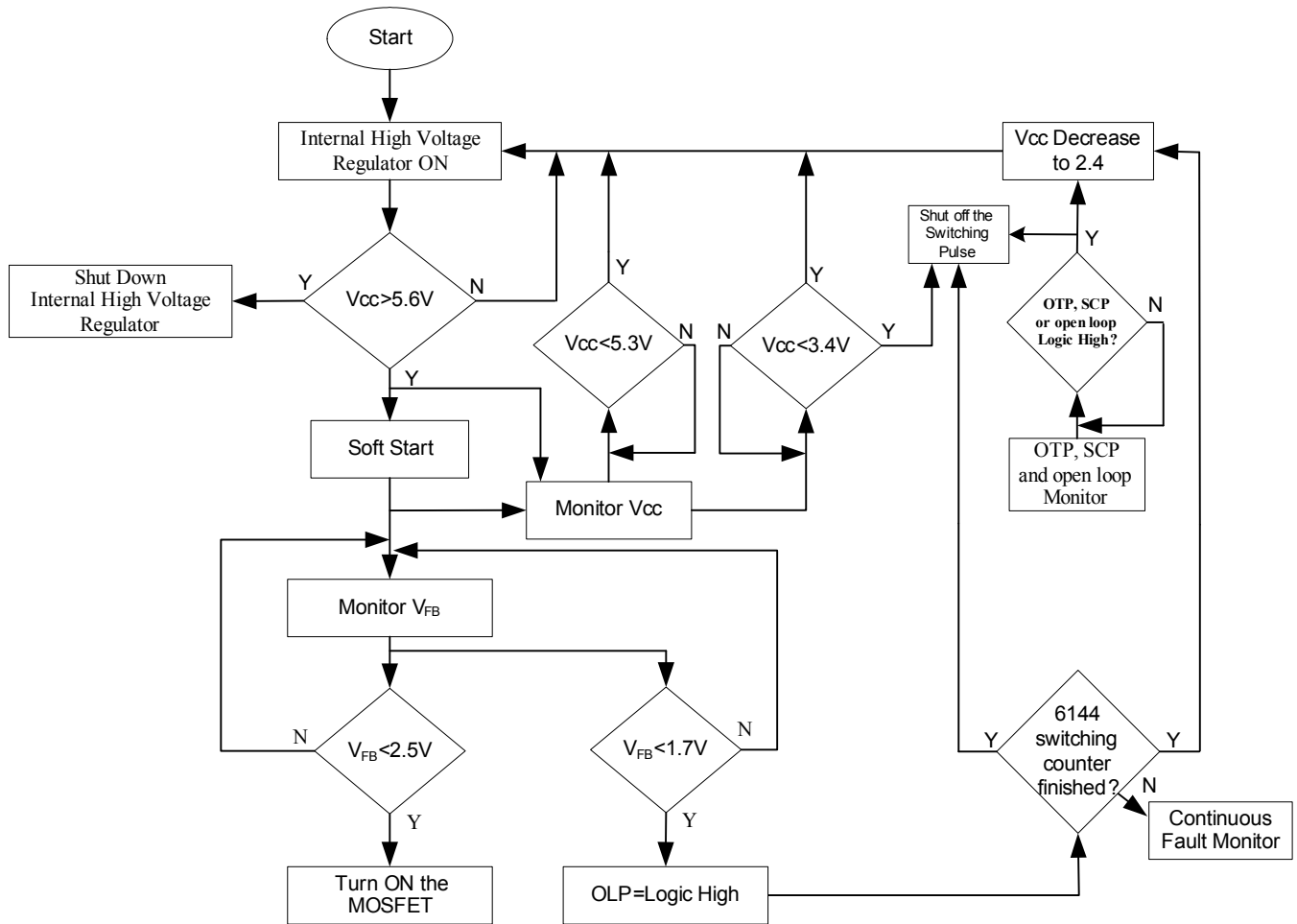
Figure 11 shows a typical application example of a 12V, 200mA non-isolated power supply using the MP155.



**Figure 11: Typical Application, 12V/200mA**



FLOW CHART



UVLO, OTP, SCP, OLP and Open Loop Protection are auto restart

Figure 12: Control Flow Chart

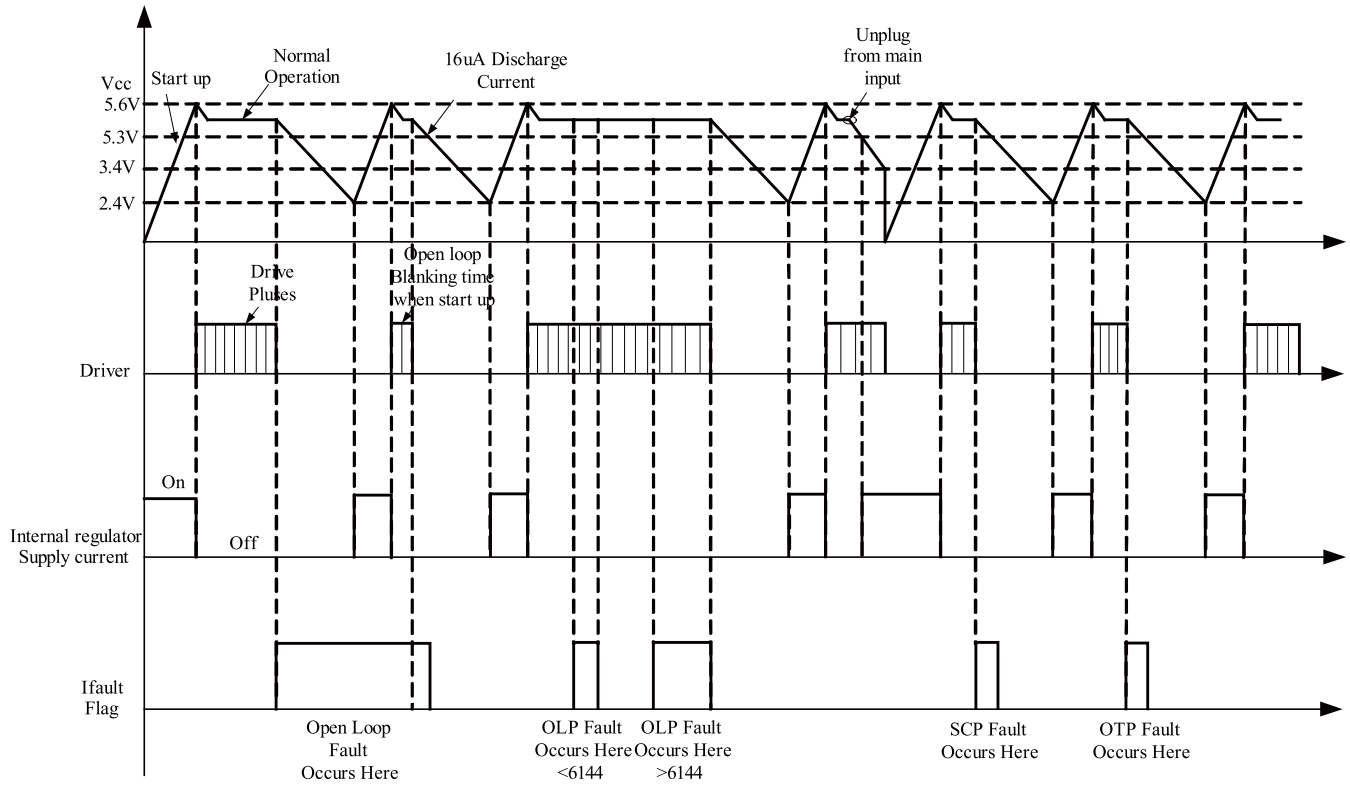
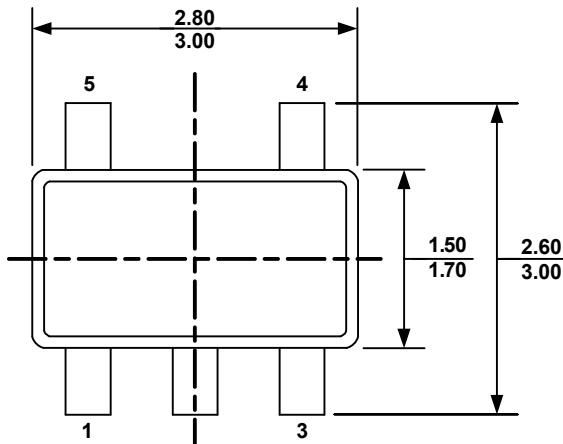


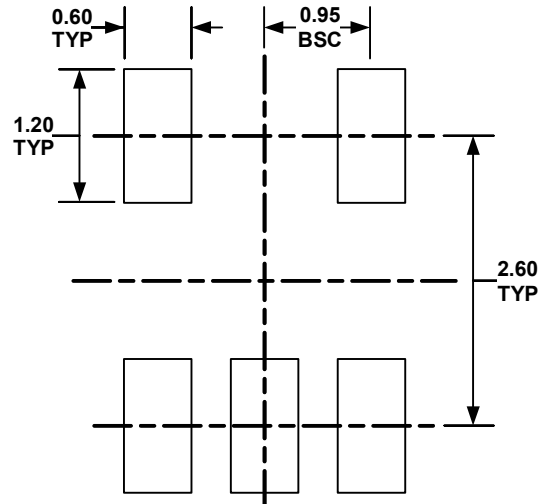
Figure 13: Signal Evolution in the Presence of a Fault

## PACKAGE INFORMATION

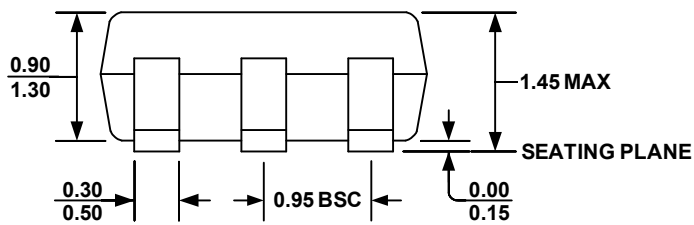
## TSOT23-5



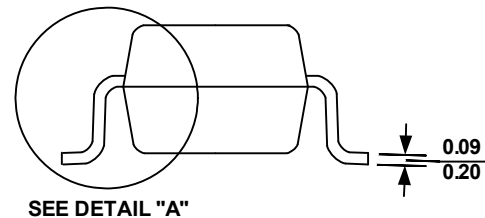
TOP VIEW



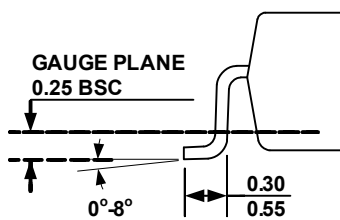
RECOMMENDED LAND PATTERN



FRONT VIEW



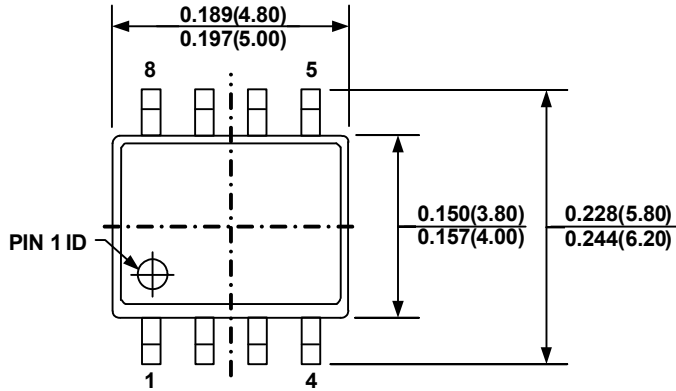
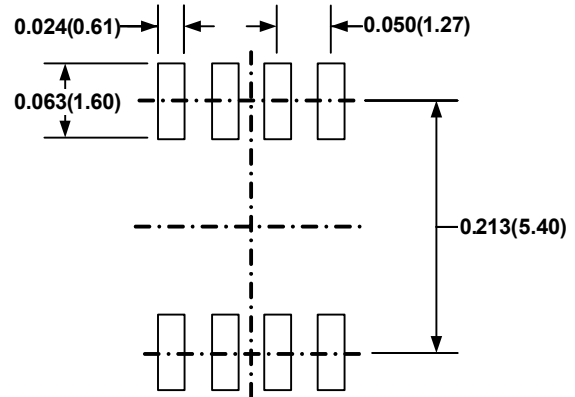
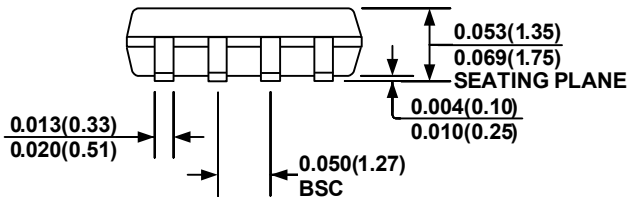
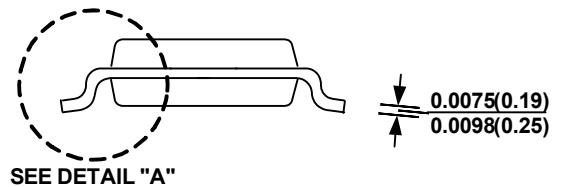
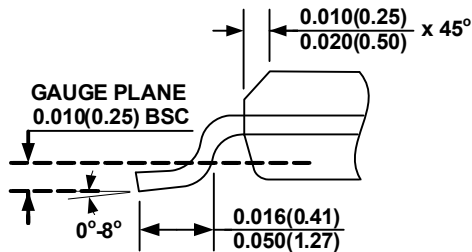
SIDE VIEW



DETAIL "A"

## NOTE:

- 1) ALL DIMENSIONS ARE IN MILLIMETERS
- 2) PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH PROTRUSION OR GATE BURR
- 3) PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION.
- 4) LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.10 MILLIMETERS MAX
- 5) DRAWING CONFORMS TO JEDEC MO-178, VARIATION AA
- 6) DRAWING IS NOT TO SCALE

**PACKAGE INFORMATION**
**SOIC8**

**TOP VIEW**

**RECOMMENDED LAND PATTERN**

**FRONT VIEW**

**SIDE VIEW**

**DETAIL "A"**
**NOTE:**

- 1) CONTROL DIMENSION IS IN INCHES DIMENSION IN BRACKET IS IN MILLIMETERS
- 2) PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH PROTRUSIONS OR GATE BURRS
- 3) PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS.
- 4) LEAD COPLANARITY(BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.004" INCHES MAX.
- 5) DRAWING CONFORMS TO JEDEC MS012, VARIATION AA
- 6) DRAWING IS NOT TO SCALE

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