

Energy Efficient Off-line Regulator

DESCRIPTION

The MP155 is a primary-side regulator that provides accurate constant voltage regulation without the opto-coupler, and supports Buck, Buck-boost, Boost and Flyback topologies. An integrated 500V MOSFET simplifies the structure and reduces costs. These features make it a competitive candidate for off-line low-power applications, such as home appliances and standby power.

The MP155 is a green-mode-operation regulator. Both the peak current and the switching frequency decrease as the load decreases. As a result, it offers excellent efficiency performance at light load, thus improving the overall average efficiency.

The MP155 features various protections such as thermal shutdown (TSD), VCC under-voltage lockout (UVLO), overload protection (OLP), short-circuit protection (SCP), and open loop protection.

The MP155 is available in the TSOT23-5 and SOIC8 packages.

FEATURES

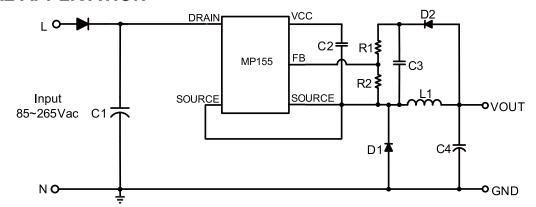
- Primary-side constant voltage (CV) control, supporting Buck, Buck-boost, Boost and Flyback topologies
- Integrated 500V/20Ω MOSFET
- < 100mW No-load power consumption
- Up to 4W output power
- Maximum DCM output current of 130mA
- Maximum CCM output current of 220mA
- Low VCC operating current
- Frequency foldback
- Maximum frequency limit
- Peak current compression
- Internal high-voltage current source
- Internal 350ns leading-edge blanking
- Thermal shutdown (auto restart)
- VCC under-voltage lockout with hysteresis (UVLO)
- Timer-based overload protection.
- Short circuit protection
- Open loop protection

APPLICATIONS

- Home Appliances, white goods and consumer electronics
- Industrial Controls
- Standby Power

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TYPICAL APPLICATION



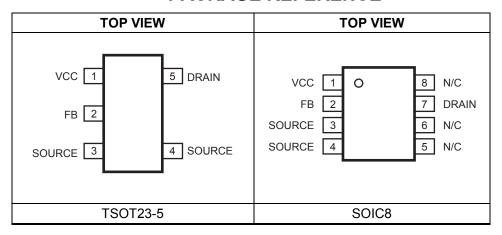


ORDERING INFORMATION

| Part Number* | Package | Top Marking |
|--------------|----------|-------------|
| MP155GJ | TSOT23-5 | AEN |
| MP155GS | SOIC8 | MP155 |

- * For Tape & Reel, add suffix –Z (e.g. MP155GJ–Z);
- * For Tape & Reel, add suffix -Z (e.g. MP155GS-Z);

PACKAGE REFERENCE



| ABSOLUTE MAXIMUM RATINGS (1) |
|---|
| Drain to SOURCE0.7V to 500V |
| All the other Pin0.7V to 6.5V |
| Continuous Power Dissipation $(T_A = +25^{\circ}C)^{(2)}$ |
| TSOT23-51W |
| SOIC81W |
| Junction Temperature 150°C |
| Lead Temperature260°C |
| Storage Temperature60°C to +150°C |
| ESD Capability Human Body Mode4.0kV |
| ESD Capability Machine Mode200V |
| (0) |

| Thermal Resistance ⁽⁴⁾ | $oldsymbol{	heta}_{JA}$ | $oldsymbol{	heta}_{JC}$ |
|-----------------------------------|-------------------------|-------------------------|
| TSOT23-5 | . 100 | 55 °C/W |
| SOIC8 | 96 | 45 °C/W |

Notes:

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature $T_J(MAX)$, the junction-to-ambient thermal resistance θ_{JA} , and the ambient temperature TA. The maximum allowance continuous power dissipation at any ambient temperature is calculated by $PD(MAX)=(TJ(MAX)-TA)/\theta_{JA}$. Exceeding the maximum allowance power dissipation will cause excessive die temperature, and the regulator will go into thermal shutdown. Internal thermal shutdown circuit protects the device from permanent damage.
- The device is not guaranteed to function outside of its operating conditions.
- 4) Measured on JESD51-7, 4-layer PCB.



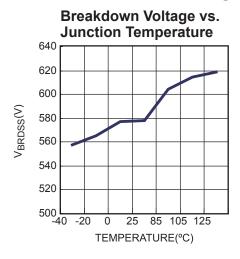
ELECTRICAL CHARACTERISTICS

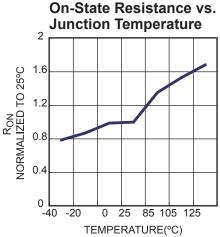
 V_{CC} = 5.8V, T_A = 25°C, unless otherwise noted.

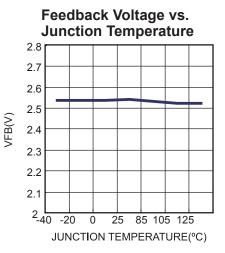
| Parameter | Symbol | Condition | Min | Тур | Max | Units |
|---|------------------------|---|-----|-----|-----|-------|
| Start-up Current Source (Drain Pin) | | | | | | |
| Internal regulator supply current | I _{regulator} | VCC=4V;V _{Drain} =100V | 2.5 | 3.5 | 4.5 | mA |
| Drain pin leakage current | I _{Leak} | VCC=5.8V;V _{Drain} =400V | | 10 | 12 | μΑ |
| Breakdown Voltage | $V_{(BR)DSS}$ | | 500 | | | V |
| Supply Voltage Management (VCC F | Pin) | | | | | |
| VCC regulator turn-off level (rising) | VCC _{OFF} | | 5.4 | 5.6 | 5.8 | V |
| VCC regulator turn-on level (falling) | VCC _{ON} | | 5.1 | 5.3 | 5.6 | V |
| On and off VCC regulator hysteresis | | | | 250 | | mV |
| VCC turn-off level (falling) | VCC _{stop} | | | 3.4 | | V |
| VCC phase completion level (falling) | VCC_{pro} | | | 2.4 | | V |
| Internal IC consumption | I _{CC} | VCC=5.8V, f _s =37kHz, D=40% | | | 430 | μΑ |
| Internal IC consumption (no switching) | I _{CC} | | | | 250 | μA |
| Internal IC Consumption, latch-off phase | I _{CCLATCH} | V _{CC} =5.3V | | 16 | | μA |
| Internal MOSFET (Drain Pin) | | | | | | |
| Breakdown voltage | V_{BRDSS} | | 500 | | | V |
| ON-State resistance | R _{on} | | | 20 | | Ω |
| Internal Current Sense | I | | | 1 | | l |
| Peak current limit | I _{Limit} | | 260 | 290 | 345 | mA |
| Leading-edge blanking | $	au_{LEB1}$ | | | 350 | | ns |
| SCP point | I _{SCP} | | | 450 | | mA |
| Leading-edge blanking for SCP | $	au_{LEB2}$ | | | 180 | | ns |
| Feedback input (FB Pin) | | <u> </u> | | | | |
| Minimum OFF time | $	au_{minoff}$ | | 15 | 18 | 21 | μs |
| Primary MOSFET feedback turn-on threshold | V _{FB} | | 2.4 | 2.5 | 2.6 | V |
| OLP feedback trigger threshold | V_{FB} OLP | | 1.6 | 1.7 | 1.8 | V |
| Over-load protection delay | $	au_{OLP}$ | f _s =37kHz | | 170 | | ms |
| Open loop detection | V _{OLD} | | | 60 | | mV |
| Thermal Shutdown | - | | | 1 | | |
| Thermal shutdown threshold | | | | 150 | | °C |
| | | | | • | | |

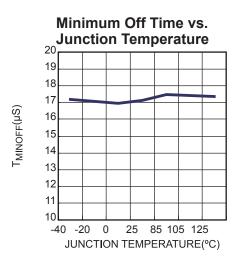


TYPICAL CHARACTERISTICS





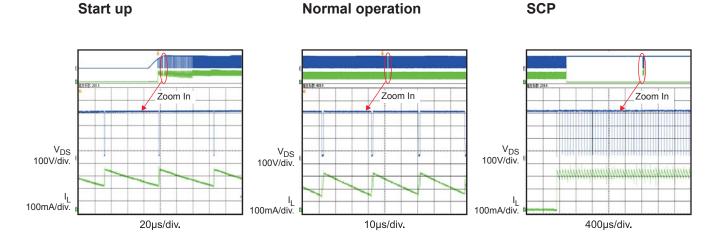




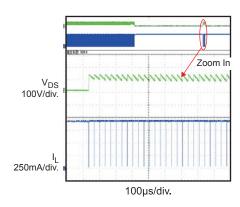


TYPICAL PERFORMANCE CHARACTERISTICS

 V_{IN} = 265VAC, V_{OUT} = 12V, I_{OUT} = 200mA, L = 2.2mH, C_{OUT} = 100 μ F, T_{A} = +25°C, unless otherwise noted.



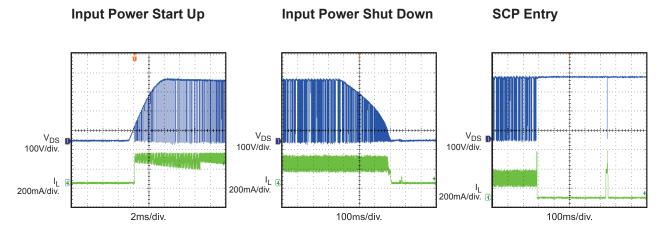
Open Loop Protection

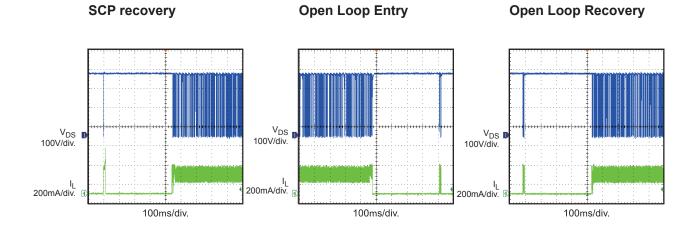




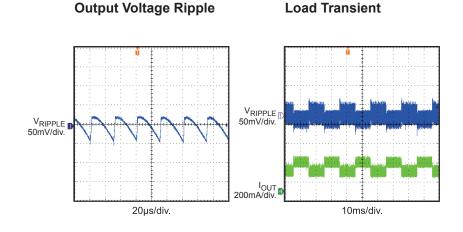
TYPICAL PERFORMANCE CHARACTERISTICS (continued)

 V_{IN} = 230VAC, V_{OUT} = 12V, I_{OUT} = 200mA, L = 2.2mH, C_{OUT} = 100 μ F, T_A = +25°C, unless otherwise noted.





Load Transient





PIN FUNCTIONS

| Pin # TSOT23-5 | Pin # SOIC8 | Name | Description |
|-------------------|----------------|--------|---|
| 1 | 1 | VCC | Control Circuit Power Supply. |
| 2 | 2 | FB | Regulator Feedback. |
| 3,4 | 3,4 | SOURCE | Internal Power MOSFET Source. Ground reference for VCC and FB pins. |
| 5 | 7 | DRAIN | Internal Power MOSFET Drain. High-voltage current source input. |
| | 5,6,8 | N/C | Not connected. |



FUNCTIONAL BLOCK DIAGRAM

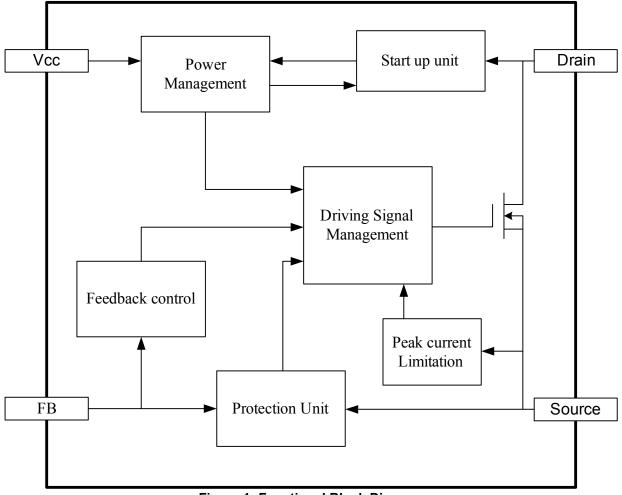


Figure 1: Functional Block Diagram



OPERATION

The MP155 is a green-mode-operation regulator. The peak current and the switching frequency both decrease as the load decreases to provide excellent efficiency at light load, and thus improve the overall average efficiency. The typical application diagram shows that the regulator operates using a minimal number of external components. It incorporates the following features:

Start-up and Under Voltage Lock-out

The internal high-voltage regulator supplies IC from the Drain pin. The IC starts switching and the internal high voltage regulator turns off when the voltage on VCC reaches 5.6V. When the VCC voltage drops below 5.3V, the internal high voltage regulator turns on again to charge the external VCC capacitor. Use a capacitor in the several μF range stabilize the VCC voltage and this can lower the cost by decreasing the value of the capacitor.

When the voltage on VCC drops blow 3.4V, the IC stops, then the internal high-voltage regulator charges the VCC capacitor.

When faults occur, such as overload, short circuit, and over-heating, the IC stops working and an internal current source (16µA) discharges the VCC capacitor. Before the VCC voltage drops below 2.4V, the internal high-voltage regulator remains off and the VCC capacitor remains discharged. Estimate the restart time after a fault as:

$$\tau_{\text{restart}} = C_{\text{VCC}} \times \frac{V_{\text{CC}} - 2.4V}{16 \text{uA}} + C_{\text{VCC}} \times \frac{5.6V - 2.4V}{3.5 \text{mA}}$$

Figure 2 shows the typical waveform with VCC under voltage lock out.

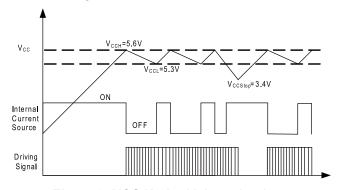


Figure 2: VCC Under-Voltage Lockout

Constant Voltage Operation

The MP155 is a fully-integrated regulator when used in a Buck solution as shown in the typical application on page 1.

The integrated MOSFET turns ON at the beginning of each cycle when the feedback voltage is below the reference voltage (2.5V). which indicates insufficient output voltage. The peak current limit determines the ON period. After the ON period elapses, the integrated MOSFET turns OFF. The freewheeling diode (D1) remains OFF until the inductor current charges the sampling capacitor (C3) voltage to the output voltage level. Then the sampling capacitor voltage changes with the output voltage. The sampling capacitor can sample and hold the output voltage to regulate the output voltage. The sampling capacitor voltage decreases after the inductor current drops below the output current. When the feedback voltage falls below the reference voltage (2.5V), a new switching cycle begins.

Figure 3 shows the detailed operation timing diagram under CCM.

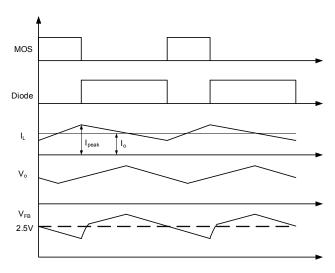


Figure 3: V_{FB} vs. V_{out}

Monitoring the sampling capacitor regulates the output voltage can be regulated, as per the following equation:

$$Vo = 2.5V \times \frac{R1 + R2}{R2}$$



Frequency Foldback

Under light load or no load conditions, the output drops very slowly, which increases the time for the MOSFET to turn ON again; i.e., frequency decreases as the load decreases. So the MP155 can maintain a high efficiency under light load condition by reducing the switching frequency automatically.

The switching frequency can be obtained as:

$$f_s = \frac{(V_{in} - V_o)}{2L(I_{peak} - I_o)} \cdot \frac{V_o}{V_{in}}, \text{ for CCM}$$

$$f_s = \frac{2(V_{in} - V_O)}{LI_{peak}^2} \cdot \frac{I_o V_o}{V_{in}}, \text{ for DCM}$$

At the same time, the peak current limit decreases from 290mA as the OFF time increases. In standby mode, the frequency and the peak current are both minimized, allowing for a small dummy load. As a result, the peak-current-compression function helps to reduce no-load consumption. Determine the peak current limitation from the following equation where τ_{off} is the power module OFF time:

$$I_{\text{Peak}} = 290\text{mA} - (1\text{mA}/\mu\text{S}) \times (\tau_{\text{off}} - 18\mu\text{S})$$

Minimum off time limitation

The MP155 implements a minimum OFF time limit. During the normal operation, the minimum OFF time limit is $18\mu s$; during start up, the minimum OFF time limit gradually drops from $72\mu s$, to $36\mu s$, then to $18\mu s$ (see Figure 4). Each minimum OFF time has 128 switching cycles. This soft-start function allows for safe start-up.

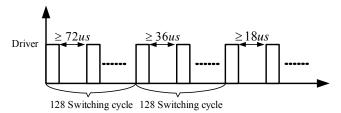


Figure 4: τ_{minoff} at Start-Up

EA Compensation

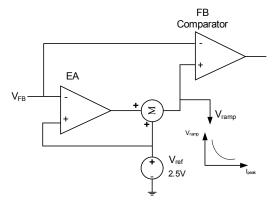


Figure 5: EA and Ramp Compensation

To improve load regulation, the MP150 implements an error amplifier (EA) compensation function (Figure 5). The MP155 samples the feedback voltage 6µs after the MOSFET turns off. EA compensation regulates the 2.5V reference voltage with the load, thus improving the power module regulation.

RAMP Compensation

An internal ramp compensation circuit precisely maintains the output voltage. An additional exponential voltage sinking source pulls down the feedback comparator's reference voltage as shown in Figure 5. The ramp compensation is relative to the load conditions: Under full-load conditions, the compensation is ~1mV/µs; with a decreasing load, the compensation increases exponentially.

Over Load Protection (OLP)

As the load increases, the peak current and the switching frequency increase with the load. When the switching frequency and peak current reaches their maximums, the output voltage will decrease if the load continues to increase. Then the FB voltage will drop below OLP threshold.

By continuously monitoring the FB voltage, the timer starts when the FB voltage drops below the 1.7V error flag threshold. Removing the error flag resets the timer. If the timer continues to completion at 170ms (f_s =37kHz), OLP occurs. This timer duration avoids triggering OLP when the power supply starts up or enters a load transition phase, and therefore requires that the power supply start up in less than 170ms. A different switching frequency (f_s) changes the over-load protection delay time, as shown below:



$$\tau_{\text{Dealy}} \approx 170 ms \times \frac{37 kHz}{fs}$$

Short Circuit Protection (SCP)

The MP155 shuts down when the peak current rises above 450mA as its short-circuit protection threshold. The power supply resumes operation after removing the fault.

Thermal shutdown (TSD)

To prevent from any lethal thermal damage, the MP150 shuts down switching when the inner temperature exceeds 150°C. During thermal shutdown (TSD), the VCC drops to 2.4V, and then the internal high voltage regulator recharges VCC.

Open Loop Detection

If the V_{FB} drops below 60mV, the IC will stop working and begins a re-start cycle. The open-loop detection is blanked for 128 switching cycles during start-up.

Leading-Edge Blanking

An internal leading-edge blanking (LEB) unit between the current sense resistor inside the IC and the current comparator input avoids prematurely switching pulse termination due to the parasitic capacitance. During the blanking period, the current comparator is disabled and cannot turn off the external MOSFET. Figure 6 shows leading-edge blanking.

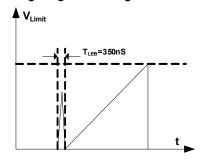
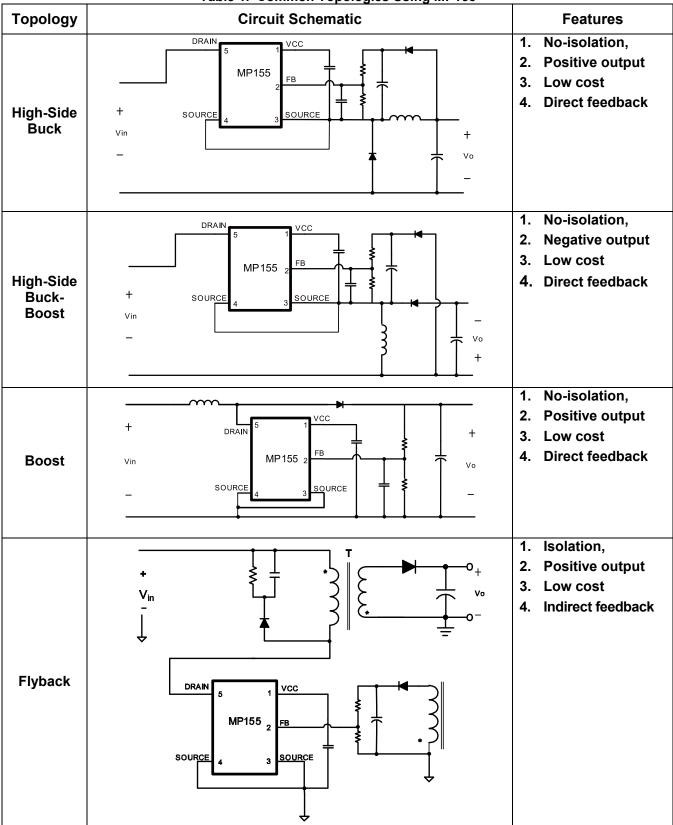


Figure 6: Leading-Edge Blanking



APPLICATION INFORMATION

Table 1. Common Topologies Using MP155





Topology Options

MP155 can be used in common topologies, such as Buck, Buck-Boost, Boost and Flyback. Please find the Table.1 for more information.

Component Selection

Input Capacitor

The input capacitor supplies the converter's DC input voltage. Figure 7 shows the typical half-wave rectifier's DC bus voltage waveform.

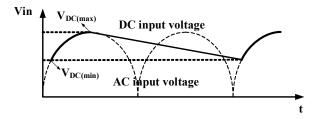


Figure 7: Input Voltage Waveform

When using the half-wave rectifier, set the input capacitor $3\mu F/W$ for the universal input condition. When using the full-wave rectifier, choose a smaller capacitor, but avoid a minimum DC voltage below 70V to avoid thermal shutdown.

Inductor

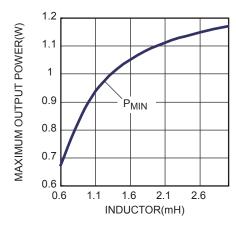
MP155 has a minimum off time limit that determines the maximum power output. The maximum power increases with the inductor value. Using a smaller inductor may cause the output to fail at full load, but a larger inductor results in a higher OLP load. The optimal inductor value is the smallest that can supply the rated power. The maximum power is:

$$P_{\text{omax}} = V_{\text{o}} (I_{\text{peak}} - \frac{V_{\text{o}} \tau_{\text{minoff}}}{2L}), \text{ for CCM}$$

$$P_{\text{omax}} = \frac{1}{2} L I_{\text{peak}}^2 \cdot \frac{1}{\tau_{\text{minoff}}}$$
 , for DCM

To account for converter parameters—such as peak current limit and minimum OFF time—estimate the minimum inductor power (P_{min}) for the maximum power, and selecting an inductor with a P_{min} value that exceeds the rated power.

Using output voltages 5V and 12V as examples, Figure 8 shows the curve for P_{min} at 5V, and Figure 9 shows the curve for P_{min} at 12V. (I_{peak} =0.29A, τ_{minoff} =18 μ s)



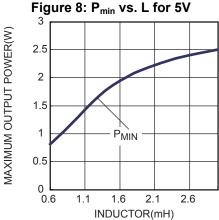


Figure 9: P_{min} vs. L for 12V

When designing a 0.5W converter (5V, 0.1A), estimate the minimum inductor value at 0.6mH based on Figure 8. Similarly, for a 1.2W converter (12V, 0.1A), estimate the minimum inductor at 0.9mH based on Figure 9.

Use a standard off-the-shelf inductor to reduce costs. Use a standard inductance that exceeds calculated inductance.

Freewheeling Diode

Choose a diode with a maximum reverse voltage rating that exceeds the maximum input voltage, and a current rating that exceeds the output current.

The reverse recovery of the freewheeling diode can affect the efficiency and circuit operation. Select an ultra-fast diode, such as the EGC10JH.



Output Capacitor

The output capacitor maintains the DC output voltage. Estimate the output voltage ripple as:

$$V_{\text{CCM_ripple}} = \frac{\Delta i}{8f_sC_o} + \Delta i \cdot R_{\text{ESR}}$$
, for CCM

$$V_{\text{DCM_ripple}} = \frac{I_o}{f_s C_o} \cdot \left(\frac{I_{pk} - I_o}{I_{pk}}\right)^2 + I_{pk} \cdot R_{\text{ESR}}, \text{ for DCM}$$

Use ceramic, tantalum, or low-ESR electrolytic capacitors to lower the output voltage ripple.

Feedback Resistors

The resistor divider determines the output voltage. Choose appropriate R1 and R2 values to maintain the FB voltage at 2.5V. Avoid very large values for R2 (typical values between $5k\Omega$ to $10k\Omega$.

Feedback Capacitor

The feedback capacitor provides a sample-andhold function. Small capacitors result in poor regulation at light load condition, and large capacitors can impact circuit operation. Estimate the capacitor range as per the following equation:

$$\frac{1}{2} \frac{V_o}{R_1 + R_2} \cdot \frac{C_o}{I_o} \le C_{FB} \le \frac{V_o}{R_1 + R_2} \cdot \frac{C_o}{I_o}$$

Choose an appropriate value given practical considerations.

Dummy Load

A dummy load maintains the load regulation. This ensures sufficient inductor energy to charge the sample-and-hold capacitor to detect the output voltage. Start with a 3mA dummy load and adjust as necessary.

VCC Supply

The MP155 obtains a low no-load power consumption by external VCC supply. This supply is dependent on the value of V_{out} . Connect a diode and resistor between C2 and C3 as per the values listed in Table 2.

Table 2: Recommended VCC Supply Resistor Values

| V_{OUT} | Resistor value | | | |
|-----------|-------------------|--|--|--|
| 3.3V | NC ⁽⁵⁾ | | | |
| 5V | NC | | | |
| 12V | 24.8k | | | |
| 16V | 40.8k | | | |
| 24V | 72.8k | | | |

Notes:

5) NC= no connection.

Surge Performance

To obtain a good surge performance, select an appropriate input capacitor that meets different surge tests. Figure 10 shows the half-wave rectifier. Table 3 shows the required capacitance under normal conditions for different surge voltages.

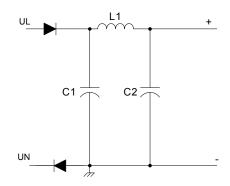


Figure 10: Half-Wave Rectifier

Table 3: Recommended Capacitor Values

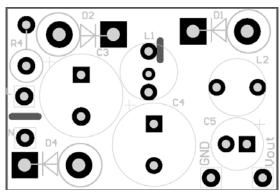
| Surge voltage | 500V | 1000V | 2000V |
|------------------|------|-------|-------|
| C1 | 1μF | 10μF | 22µF |
| C2 | 1µF | 4.7µF | 10μF |



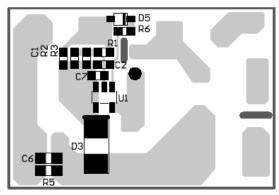
Layout Guide

PCB layout is very important to achieve reliable operation, and good EMI and thermal performance. Follow these guidelines to optimize performance.

- 1) Minimize the loop area formed by the input capacitor, IC part, freewheeling diode, inductor and output capacitor.
- 2) Place the power inductor far away from the input filter.
- 3) Add a capacitor in the several-hundred pF range between pin FB and source as close to the IC as possible.
- 4) Connect the exposed pad with the Drain pin to a large copper area to improve thermal performance.



Top



Bottom Layer

Design Example

Below is a design example following the application guidelines given the following specifications:

Table 4: Design Example

| V_{IN} | 85 to 265Vac |
|------------------|--------------|
| V _{out} | 12V |
| I _{out} | 200mA |

Figure 11 shows the detailed application schematic. The Typical Performance Characteristics section lists typical performance and circuit waveforms. For more device application, please refer to the related Evaluation Board Datasheets.



TYPICAL APPLICATION CIRCUITS

Figure 11 shows a typical application example of a 12V, 200mA non-isolated power supply using the MP155.

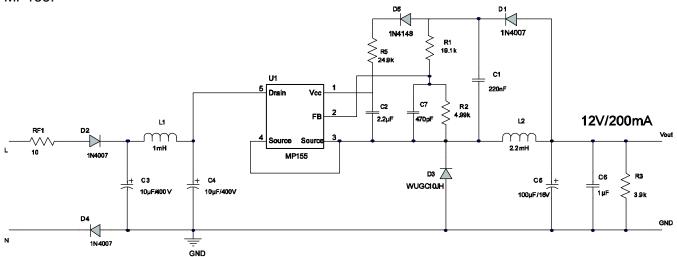
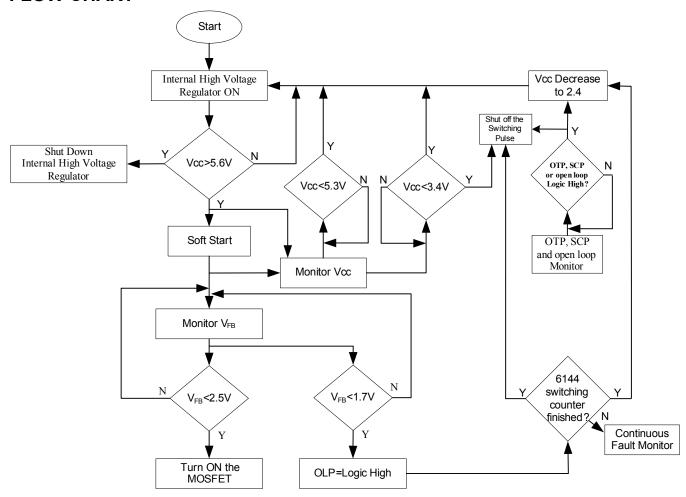


Figure 11: Typical Application, 12V/200mA



FLOW CHART



UVLO, OTP, SCP, OLP and Open Loop Protection are auto restar

Figure 12: Control Flow Chart



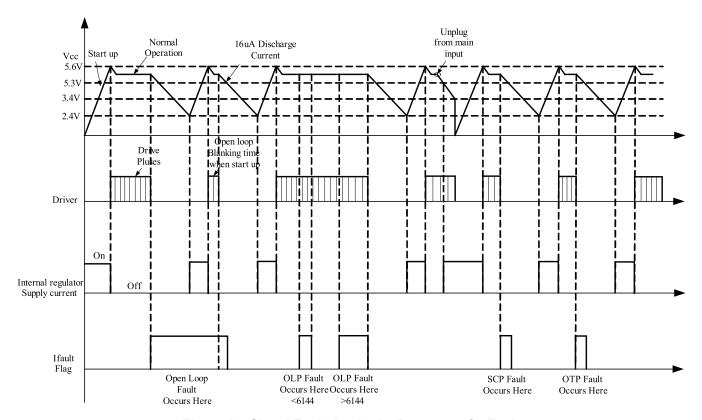
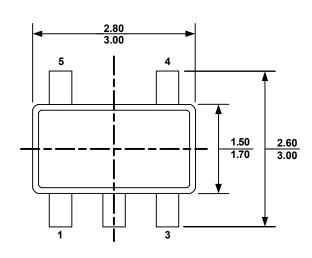


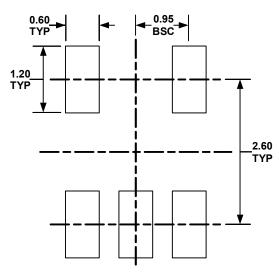
Figure 13: Signal Evolution in the Presence of a Fault



PACKAGE INFORMATION

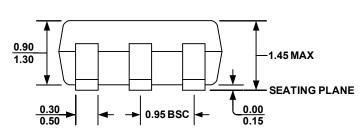
TSOT23-5

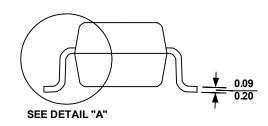




TOP VIEW

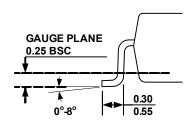
RECOMMENDED LAND PATTERN





FRONT VIEW

SIDE VIEW



DETAIL "A"

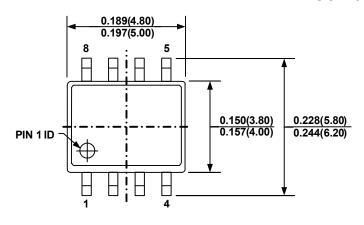
NOTE:

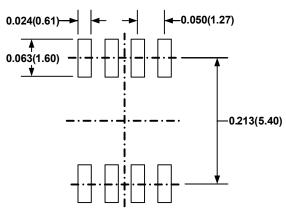
- 1) ALL DIMENSIONS ARE IN MILLIMETERS
- 2) PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH PROTRUSION OR GATE BURR
- 3) PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION.
- 4) LEAD COPLANARITY(BOTTOM OF LEADS AFTER FORMING SHALL BE0.10 MILLIMETERS MAX
- 5) DRAWING CONFORMS TO JEDEC MO-178, VARIATION AA
- 6) DRAWING IS NOT TO SCALE



PACKAGE INFORMATION

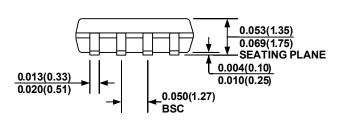
SOIC8



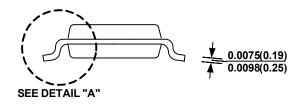


TOP VIEW

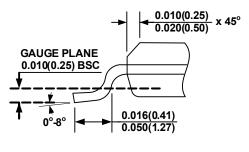
RECOMMENDED LAND PATTERN



FRONT VIEW



SIDE VIEW



DETAIL "A"

NOTE:

- 1) CONTROL DIMENSION IS IN INCHES DIMENSION IN BRACKET IS IN MILLIMETERS
- 2) PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH PROTRUSIONS OR GATE BURRS
- 3) PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS.
- 4) LEAD COPLANARITY(BOTTOM OF LEADS AFTER FORMING SHALL BE0.004" INCHES MAX.
- 5) DRAWING CONFORMS TO JEDEC MS012, VARIATION AA
- 6) DRAWING IS NOT TO SCALE

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OOO «ЛайфЭлектроникс" "LifeElectronics" LLC

ИНН 7805602321 КПП 780501001 P/C 40702810122510004610 ФАКБ "АБСОЛЮТ БАНК" (ЗАО) в г.Санкт-Петербурге К/С 3010181090000000703 БИК 044030703

Компания «Life Electronics» занимается поставками электронных компонентов импортного и отечественного производства от производителей и со складов крупных дистрибьюторов Европы, Америки и Азии.

С конца 2013 года компания активно расширяет линейку поставок компонентов по направлению коаксиальный кабель, кварцевые генераторы и конденсаторы (керамические, пленочные, электролитические), за счёт заключения дистрибьюторских договоров

Мы предлагаем:

- Конкурентоспособные цены и скидки постоянным клиентам.
- Специальные условия для постоянных клиентов.
- Подбор аналогов.
- Поставку компонентов в любых объемах, удовлетворяющих вашим потребностям.
- Приемлемые сроки поставки, возможна ускоренная поставка.
- Доставку товара в любую точку России и стран СНГ.
- Комплексную поставку.
- Работу по проектам и поставку образцов.
- Формирование склада под заказчика.
- Сертификаты соответствия на поставляемую продукцию (по желанию клиента).
- Тестирование поставляемой продукции.
- Поставку компонентов, требующих военную и космическую приемку.
- Входной контроль качества.
- Наличие сертификата ISO.

В составе нашей компании организован Конструкторский отдел, призванный помогать разработчикам, и инженерам.

Конструкторский отдел помогает осуществить:

- Регистрацию проекта у производителя компонентов.
- Техническую поддержку проекта.
- Защиту от снятия компонента с производства.
- Оценку стоимости проекта по компонентам.
- Изготовление тестовой платы монтаж и пусконаладочные работы.



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