

### FEATURES

- Low noise: 1.1 nV/ $\sqrt{\text{Hz}}$  at 1 kHz
- Low distortion:  $-120$  dB THD @ 1 kHz
- Input noise, 0.1 Hz to 10 Hz:  $<76$  nV p-p
- Slew rate: 14 V/ $\mu\text{s}$
- Wide bandwidth: 10 MHz
- Supply current: 4.8 mA/amp typical
- Low offset voltage: 10  $\mu\text{V}$  typical
- CMRR: 120 dB
- Unity-gain stable
- $\pm 15$  V operation

### APPLICATIONS

- Professional audio preamplifiers
- ATE/precision testers
- Imaging systems
- Medical/physiological measurements
- Precision detectors/instruments
- Precision data conversion

### GENERAL DESCRIPTION

The AD8597/AD8599 are very low noise, low distortion operational amplifiers ideal for use as preamplifiers. The low noise of 1.1 nV/ $\sqrt{\text{Hz}}$  and low harmonic distortion of  $-120$  dB (or better) at audio bandwidths give the AD8597/AD8599 the wide dynamic range necessary for preamplifiers in audio, medical, and instrumentation applications. The excellent slew rate of 14 V/ $\mu\text{s}$  and 10 MHz gain bandwidth make them highly suitable for medical applications. The low distortion and fast settling time make them ideal for buffering of high resolution data converters.

### PIN CONFIGURATIONS

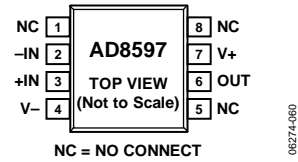


Figure 1. AD8597 8-Lead SOIC (R-8)

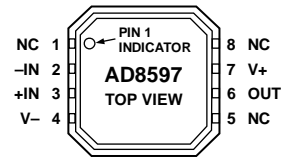


Figure 2. AD8597 8-Lead LFCSP (CP-8-2)

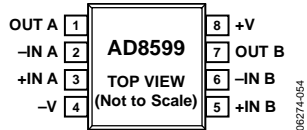


Figure 3. AD8599 8-Lead SOIC (R-8)

The AD8597 is available in 8-lead SOIC and LFCSP packages, while the AD8599 is available in an 8-lead SOIC package. They are both specified over a  $-40^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$  temperature range. The AD8597 and AD8599 are members of a growing series of low noise op amps offered by Analog Devices, Inc., (see Table 1).

Table 1. Low Noise Op Amps

Package	0.9 nV	1.1 nV	1.8 nV	2.8 nV	3.8 nV
Single	AD797	AD8597	ADA4004-1	AD8675	AD8671
Dual		AD8599	ADA4004-2	AD8676	AD8672
Quad			ADA4004-4		AD8674

## TABLE OF CONTENTS

Features .....	1	ESD Caution.....	5
Applications.....	1	Typical Performance Characteristics .....	6
Pin Configurations .....	1	Functional Operation.....	15
General Description .....	1	Input Voltage Range.....	15
Revision History .....	2	Output Phase Reversal.....	15
Specifications.....	3	Noise and Source Impedance Considerations .....	15
Absolute Maximum Ratings.....	5	Outline Dimensions .....	17
Thermal Resistance .....	5	Ordering Guide .....	17
Power Sequencing .....	5		

## REVISION HISTORY

### 2/13—Rev. C to Rev. D

Changes to Figure 44 .....	12
Changes to Figure 46 and Figure 49.....	13

### 12/09—Rev. B to Rev. C

Changes to Table 1 .....	1
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### 10/08—Rev. A to Rev. B

Added AD8597 .....	Universal
Added LFCSP_VD .....	Universal
Added Table 1.....	1
Changes to Specifications Section .....	3
Changes to Absolute Maximum Ratings Section .....	5
Changes to Typical Performance Characteristics Section.....	6
Added Figure 12 and Figure 15.....	7
Added Figure 18 and Figure 19.....	8
Added Figure 30 and Figure 33.....	10

Added Figure 34 to Figure 38 .....	11
Added Figure 42 and Figure 45 .....	12
Added Figure 52, Figure 55, Figure 57 .....	14
Added Functional Operation Section.....	15
Added Figure 58 .....	15
Updated Outline Dimensions .....	17
Changes to Ordering Guide .....	17

### 4/07—Rev. 0 to Rev. A

Updated Layout .....	5
Changes to Figure 45 Caption .....	12
Added Figure 48 .....	12
Changes to Figure 51 Caption .....	13

### 2/07—Revision 0: Initial Version

## SPECIFICATIONS

$V_{SY} = \pm 5\text{ V}$ ,  $V_{CM} = 0\text{ V}$ ,  $V_O = 0\text{ V}$ ,  $T_A = 25^\circ\text{C}$ , unless otherwise specified.

Table 2.

Parameter	Symbol	Conditions	Min	Typ	Max	Unit
<b>INPUT CHARACTERISTICS</b>						
Offset Voltage	$V_{OS}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		15	120	$\mu\text{V}$
					180	$\mu\text{V}$
Offset Voltage Drift	$\Delta V_{OS}/\Delta T$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		0.8	2.2	$\mu\text{V}/^\circ\text{C}$
Input Bias Current	$I_B$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		40	210	nA
					340	nA
Input Offset Current	$I_{OS}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		65	250	nA
					340	nA
Input Voltage Range	IVR		-2.0		+2.0	V
Common-Mode Rejection Ratio	CMRR	$-2.0\text{ V} \leq V_{CM} \leq +2.0\text{ V}$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	120	135		dB
			105			dB
Large Signal Voltage Gain	$A_{VO}$	$R_L \geq 600\ \Omega$ , $V_O = -11\text{ V to } +11\text{ V}$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	105	110		dB
			100			dB
Input Capacitance						
Differential Capacitance	$C_{DIFF}$			15.4		pF
Common-Mode Capacitance	$C_{CM}$			5.5		pF
<b>OUTPUT CHARACTERISTICS</b>						
Output Voltage High	$V_{OH}$	$R_L = 600\ \Omega$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	3.5	3.7		V
			3.3			V
		$R_L = 2\ \text{k}\Omega$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	3.7	3.8		V
			3.5			V
Output Voltage Low	$V_{OL}$	$R_L = 600\ \Omega$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		-3.6	-3.4	V
					-3.3	V
		$R_L = 2\ \text{k}\Omega$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		-3.7	-3.5	V
					-3.4	V
Output Short-Circuit Current	$I_{SC}$			$\pm 52$		mA
Closed-Loop Output Impedance	$Z_{OUT}$	At 1 MHz, $A_V = 1$		5		$\Omega$
<b>POWER SUPPLY</b>						
Power Supply Rejection Ratio	PSRR	$V_{SY} = \pm 18\text{ V to } \pm 4.5\text{ V}$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	120	140		dB
			118			dB
Supply Current per Amplifier	$I_{SY}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		4.8	5.5	mA
					6.5	mA
<b>DYNAMIC PERFORMANCE</b>						
Slew Rate	SR	$A_V = -1$ , $R_L = 2\ \text{k}\Omega$ $A_V = 1$ , $R_L = 2\ \text{k}\Omega$		14		V/ $\mu\text{s}$
				14		V/ $\mu\text{s}$
Settling Time	$t_S$	To 0.01%, step = 10 V		2		$\mu\text{s}$
Gain Bandwidth Product	GBP			10		MHz
Phase Margin	$\Phi_M$			60		Degrees
<b>NOISE PERFORMANCE</b>						
Peak-to-Peak Noise	$e_n$ p-p	0.1 Hz to 10 Hz		76		nV p-p
Voltage Noise Density	$e_n$	$f = 1\ \text{kHz}$		1.07	1.15	nV/ $\sqrt{\text{Hz}}$
		$f = 10\ \text{Hz}$			1.5	nV/ $\sqrt{\text{Hz}}$
Correlated Current Noise		$f = 1\ \text{kHz}$		2.0		pA/ $\sqrt{\text{Hz}}$
		$f = 10\ \text{Hz}$		4.2		pA/ $\sqrt{\text{Hz}}$
Uncorrelated Current Noise		$f = 1\ \text{kHz}$		2.4		pA/ $\sqrt{\text{Hz}}$
		$f = 10\ \text{Hz}$		5.2		pA/ $\sqrt{\text{Hz}}$
Total Harmonic Distortion + Noise	THD + N	$G = 1$ , $R_L \geq 1\ \text{k}\Omega$ , $f = 1\ \text{kHz}$ , $V_{RMS} = 1\text{ V}$		-120		dB
Channel Separation	CS	$f = 10\ \text{kHz}$		-120		dB

$V_S = \pm 15\text{ V}$ ,  $V_{CM} = 0\text{ V}$ ,  $V_O = 0\text{ V}$ ,  $T_A = +25^\circ\text{C}$ , unless otherwise specified.

Table 3.

Parameter	Symbol	Conditions	Min	Typ	Max	Unit
<b>INPUT CHARACTERISTICS</b>						
Offset Voltage	$V_{OS}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		10	120	$\mu\text{V}$
					180	$\mu\text{V}$
Offset Voltage Drift	$\Delta V_{OS}/\Delta T$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		0.8	2.2	$\mu\text{V}/^\circ\text{C}$
Input Bias Current	$I_B$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		25	200	nA
					300	nA
Input Offset Current	$I_{OS}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		50	200	nA
					300	nA
Input Voltage Range	IVR		-12.5		+12.5	V
Common-Mode Rejection Ratio	CMRR	$-12.5\text{ V} \leq V_{CM} \leq +12.5\text{ V}$	120	135		dB
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	115			dB
Large Signal Voltage Gain	$A_{VO}$	$R_L \geq 600\ \Omega$ , $V_O = -11\text{ V to } +11\text{ V}$	110	116		dB
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	106			dB
Input Capacitance						
Differential Capacitance	$C_{DIFF}$			12.1		pF
Common-Mode Capacitance	$C_{CM}$			5.1		pF
<b>OUTPUT CHARACTERISTICS</b>						
Output Voltage High	$V_{OH}$	$R_L = 600\ \Omega$	13.1	13.4		V
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	12.8			V
		$R_L = 2\text{ k}\Omega$	13.5	13.7		V
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	13.2			V
Output Voltage Low	$V_{OL}$	$R_L = 600\ \Omega$		-13.2	-12.9	V
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			-12.8	V
		$R_L = 2\text{ k}\Omega$		-13.5	-13.4	V
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			-13.3	V
Output Short-Circuit Current	$I_{SC}$			$\pm 52$		mA
Closed-Loop Output Impedance	$Z_{OUT}$	At 1 MHz, $A_V = 1$		5		$\Omega$
<b>POWER SUPPLY</b>						
Power Supply Rejection Ratio	PSRR	$V_{SY} = \pm 18\text{ V to } \pm 4.5\text{ V}$	120	140		dB
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	118			dB
Supply Current per Amplifier	$I_{SY}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		5.0	5.7	mA
					6.75	mA
<b>DYNAMIC PERFORMANCE</b>						
Slew Rate	SR	$A_V = -1$ , $R_L = 2\text{ k}\Omega$		16		V/ $\mu\text{s}$
		$A_V = 1$ , $R_L = 2\text{ k}\Omega$		15		V/ $\mu\text{s}$
Settling Time	$t_s$	To 0.01%, step = 10 V		2		$\mu\text{s}$
Gain Bandwidth Product	GBP			10		MHz
Phase Margin	$\Phi_M$			65		Degrees
<b>NOISE PERFORMANCE</b>						
Peak-to-Peak Noise	$e_n$ p-p	0.1 Hz to 10 Hz		76		nV p-p
Voltage Noise Density	$e_n$	$f = 1\text{ kHz}$		1.07	1.15	nV/ $\sqrt{\text{Hz}}$
		$f = 10\text{ Hz}$			1.5	nV/ $\sqrt{\text{Hz}}$
Correlated Current Noise		$f = 1\text{ kHz}$		1.9		pA/ $\sqrt{\text{Hz}}$
		$f = 10\text{ Hz}$		4.3		pA/ $\sqrt{\text{Hz}}$
Uncorrelated Current Noise		$f = 1\text{ kHz}$		2.3		pA/ $\sqrt{\text{Hz}}$
		$f = 10\text{ Hz}$		5.3		pA/ $\sqrt{\text{Hz}}$
Total Harmonic Distortion + Noise	THD + N	$G = 1$ , $R_L \geq 1\text{ k}\Omega$ , $f = 1\text{ kHz}$ , $V_{RMS} = 3\text{ V}$		-120		dB
Channel Separation	CS	$f = 10\text{ kHz}$		-120		dB

## ABSOLUTE MAXIMUM RATINGS

Table 4.

Parameter	Rating
Supply Voltage	$\pm 18\text{ V}$
Input Voltage	$-V \leq V_{IN} \leq +V$
Differential Input Voltage <sup>1</sup>	$\pm 1\text{ V}$
Output Short-Circuit to GND	Indefinite
Storage Temperature Range	$-65^{\circ}\text{C}$ to $+150^{\circ}\text{C}$
Operating Temperature Range	$-40^{\circ}\text{C}$ to $+125^{\circ}\text{C}$
Lead Temperature Range (Soldering 60 sec)	$300^{\circ}\text{C}$
Junction Temperature	$150^{\circ}\text{C}$

<sup>1</sup> If the differential input voltage exceeds 1 V, the current should be limited to 5 mA.

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## THERMAL RESISTANCE

$\theta_{JA}$  is specified with the device soldered on a circuit board with its exposed paddle soldered to a pad (if applicable) on a 4-layer JEDEC standard PCB with zero air flow.

Table 5.

Package Type	$\theta_{JA}$	$\theta_{JC}$	Unit
8-Lead LFCSP_VD (CP-8-2)	78	20	$^{\circ}\text{C}/\text{W}$
8-Lead SOIC (R-8) (AD8597)	140	39	$^{\circ}\text{C}/\text{W}$
8-Lead SOIC (R-8) (AD8599)	120	36	$^{\circ}\text{C}/\text{W}$

## POWER SEQUENCING

The op amp supplies should be applied simultaneously. The op amp supplies should be stable before any input signals are applied. In any case, the input current must be limited to 5 mA.

## ESD CAUTION



**ESD (electrostatic discharge) sensitive device.** Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

TYPICAL PERFORMANCE CHARACTERISTICS

T<sub>A</sub> = 25°C, unless otherwise noted.

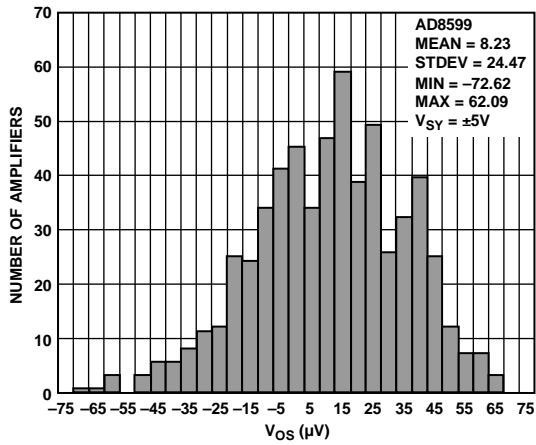


Figure 4. Input Offset Voltage Distribution

06274-001

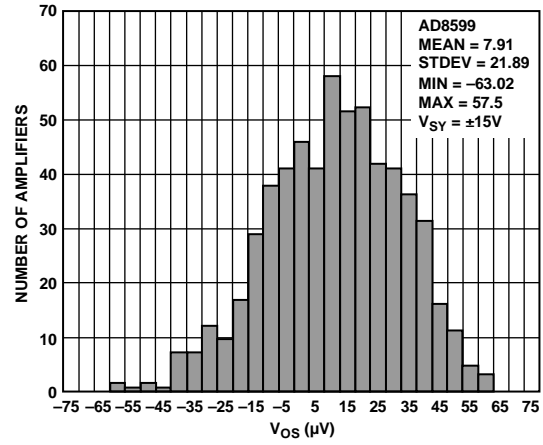


Figure 7. Input Offset Voltage Distribution

06274-002

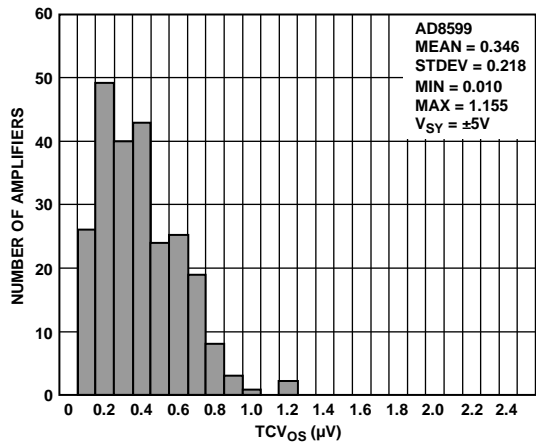


Figure 5. TCV<sub>OS</sub> Distribution, -40°C ≤ T<sub>A</sub> ≤ +125°C

06274-004

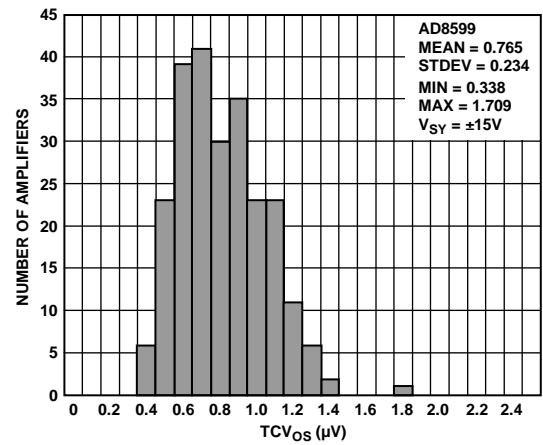


Figure 8. TCV<sub>OS</sub> Distribution, -40°C ≤ T<sub>A</sub> ≤ +125°C

06274-007

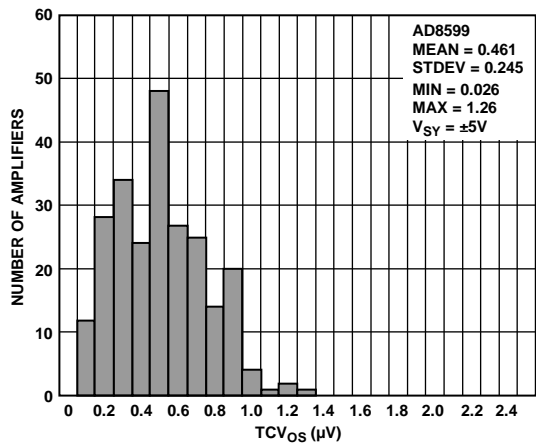


Figure 6. TCV<sub>OS</sub> Distribution, -40°C ≤ T<sub>A</sub> ≤ +85°C

06274-006

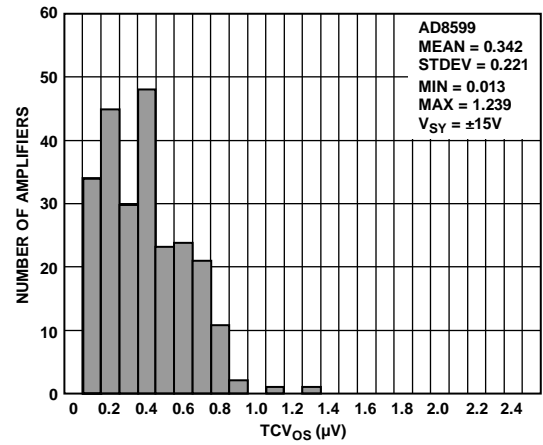


Figure 9. TCV<sub>OS</sub> Distribution, -40°C ≤ T<sub>A</sub> ≤ +85°C

06274-005

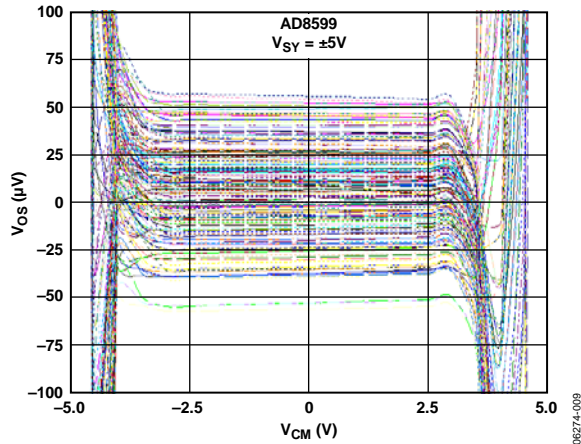


Figure 10. Offset Voltage vs.  $V_{CM}$

06274-009

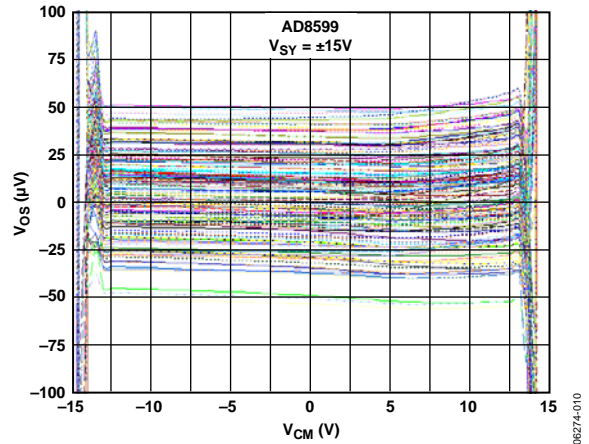


Figure 13. Offset Voltage vs.  $V_{CM}$

06274-010

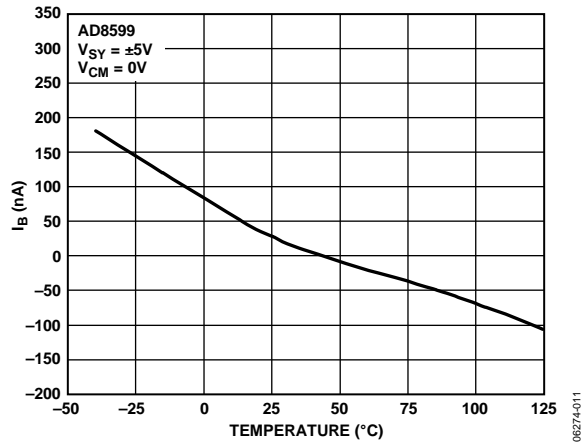


Figure 11. Input Bias Current vs. Temperature

06274-011

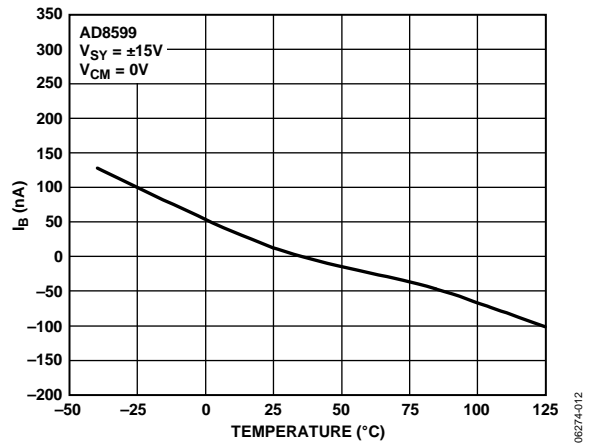


Figure 14. Input Bias Current vs. Temperature

06274-012

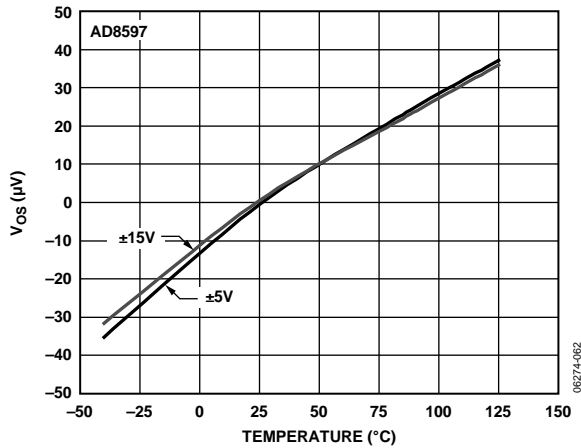


Figure 12. Input Offset Voltage vs. Temperature

06274-062

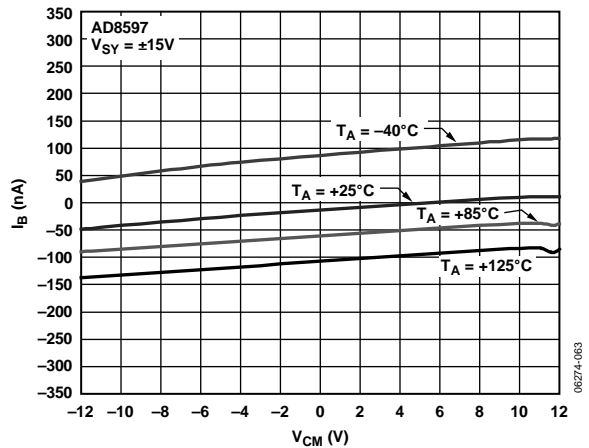


Figure 15. Input Bias Current vs. Temperature

06274-063

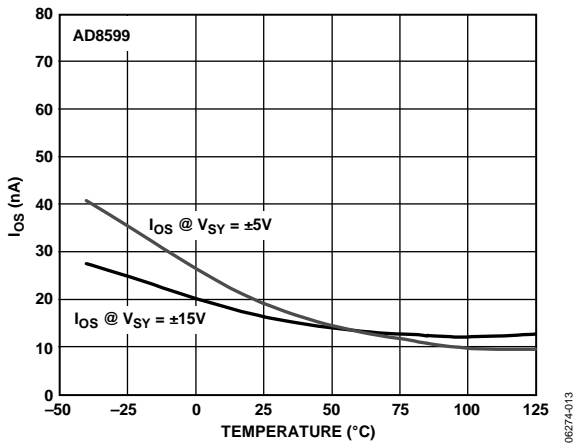


Figure 16. Input Offset Current vs. Temperature

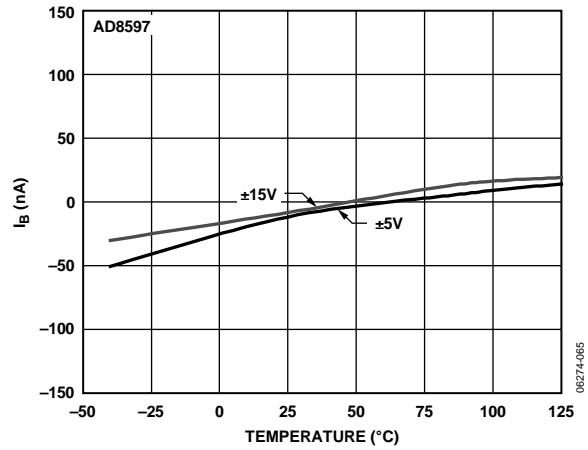


Figure 19. Input Offset Current vs. Temperature

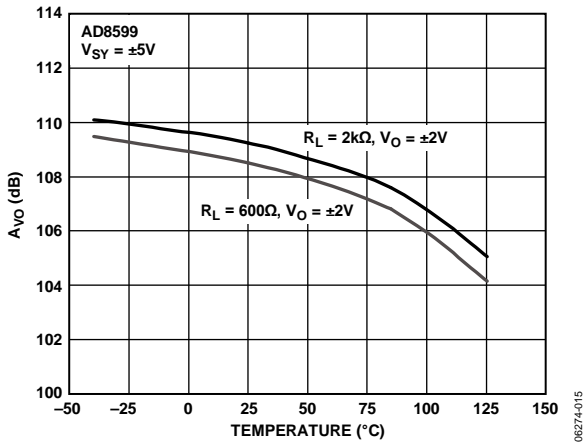


Figure 17. Large Signal Voltage Gain vs. Temperature

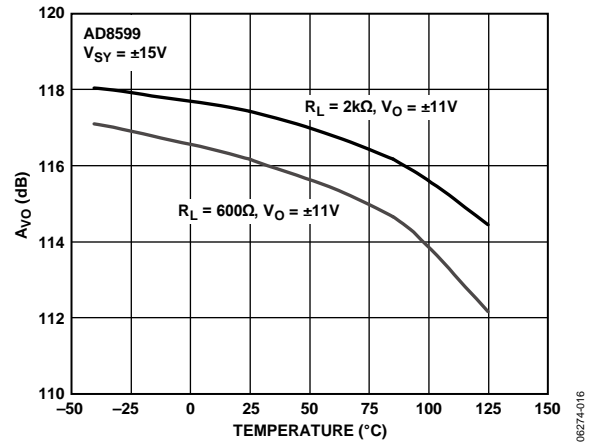


Figure 20. Large Signal Voltage Gain vs. Temperature

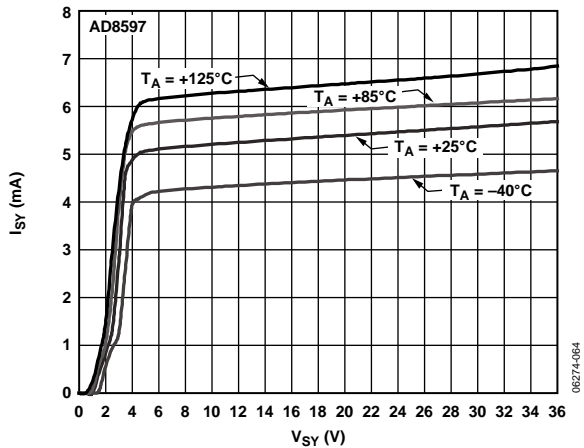


Figure 18. Supply Current vs. Supply Voltage

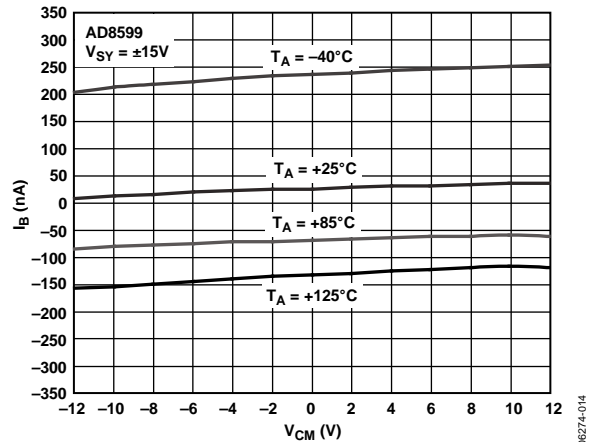


Figure 21. Input Bias Current vs.  $V_{CM}$



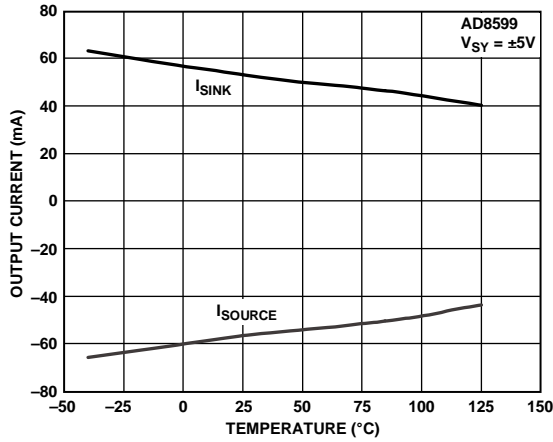


Figure 22.  $I_{sc}$  vs. Temperature

06274-017

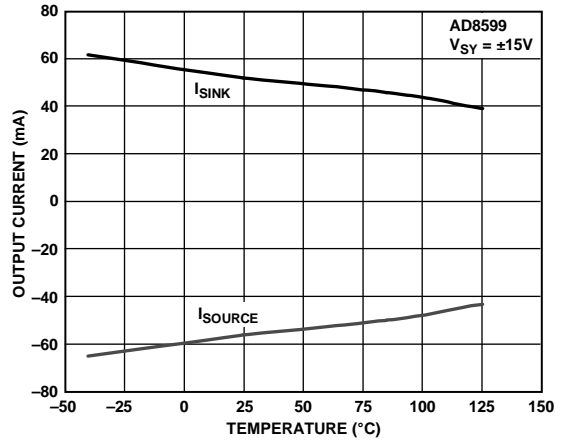


Figure 25.  $I_{sc}$  vs. Temperature

06274-018

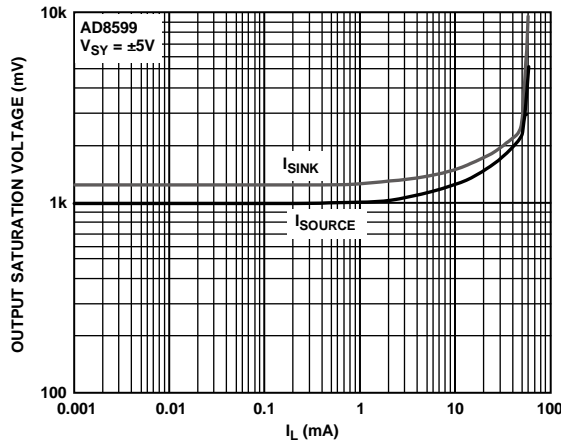


Figure 23. Output Saturation Voltage vs. Current Load

06274-021

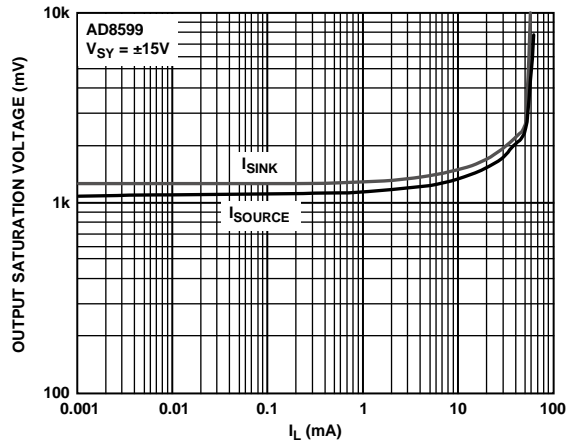


Figure 26. Output Saturation Voltage vs. Current Load

06274-022

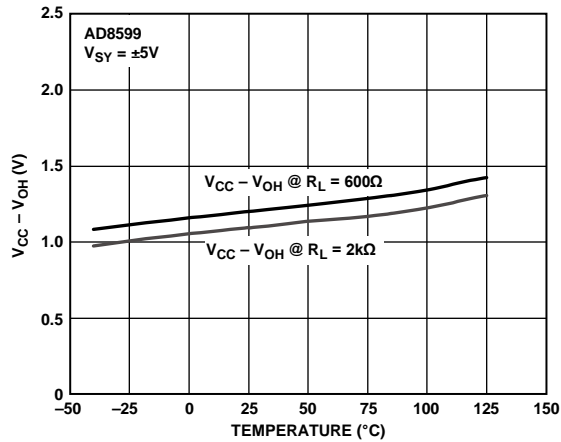


Figure 24. Output Saturation Voltage vs. Temperature

06274-027

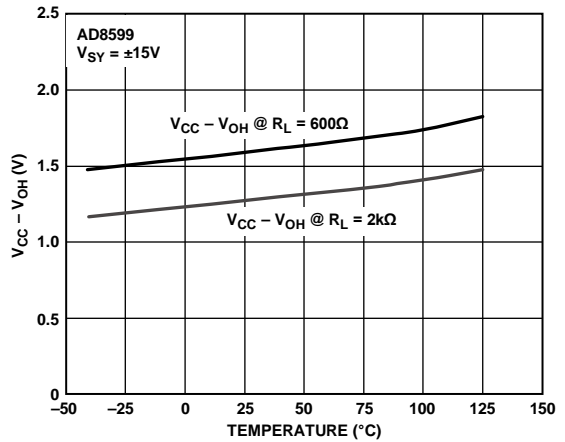


Figure 27. Output Saturation Voltage vs. Temperature

06274-029

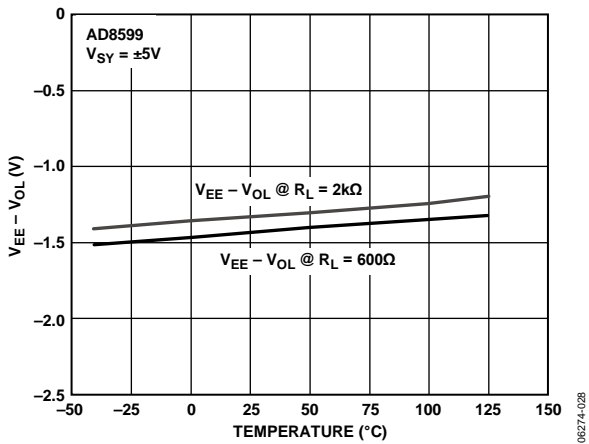


Figure 28. Output Saturation Voltage vs. Temperature

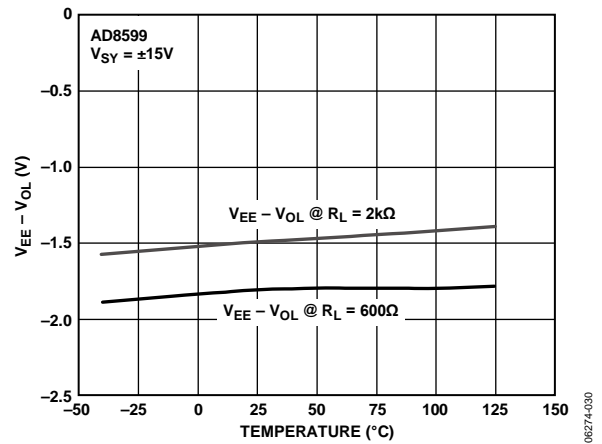


Figure 31. Output Saturation Voltage vs. Temperature

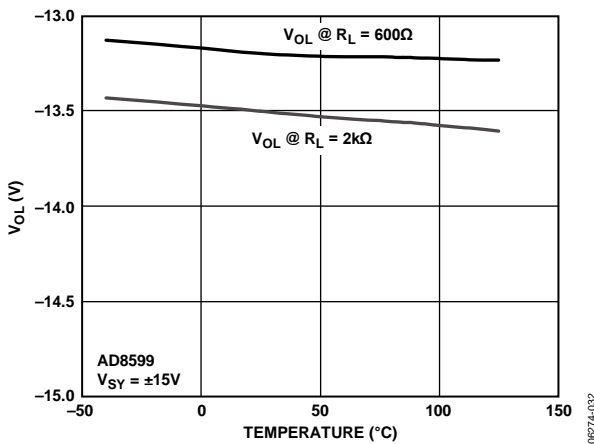


Figure 29. Output Voltage Low vs. Temperature

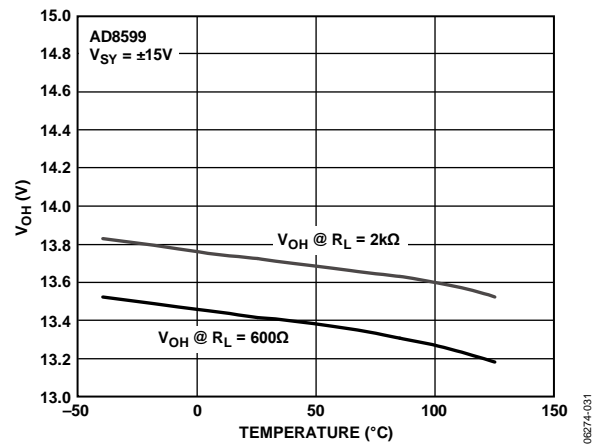


Figure 32. Output Voltage High vs. Temperature

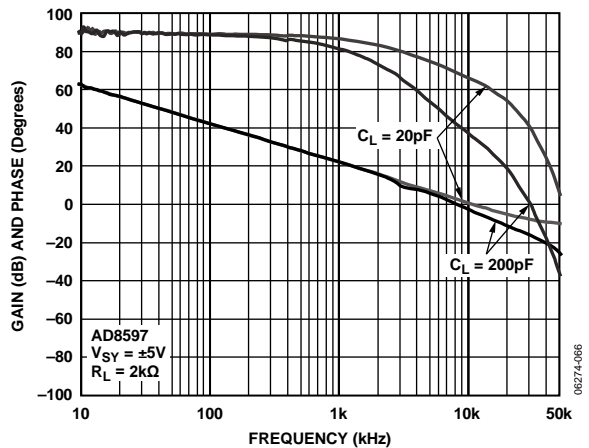


Figure 30. Gain and Phase vs. Frequency

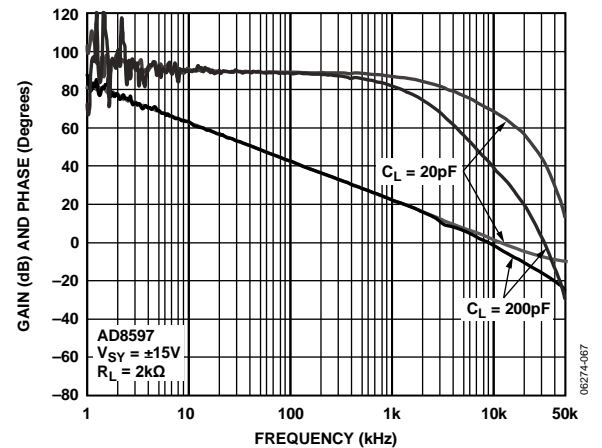


Figure 33. Gain and Phase vs. Frequency

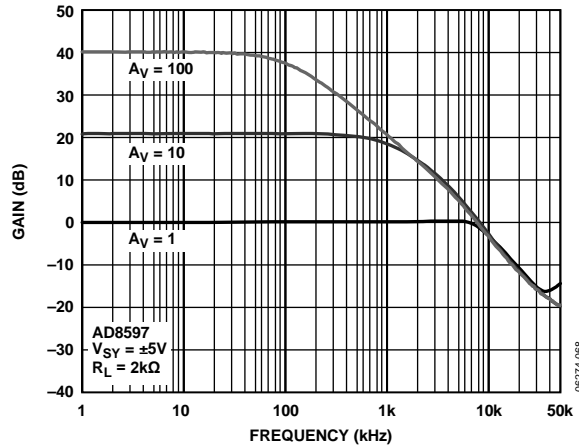


Figure 34. Closed-Loop Gain vs. Frequency

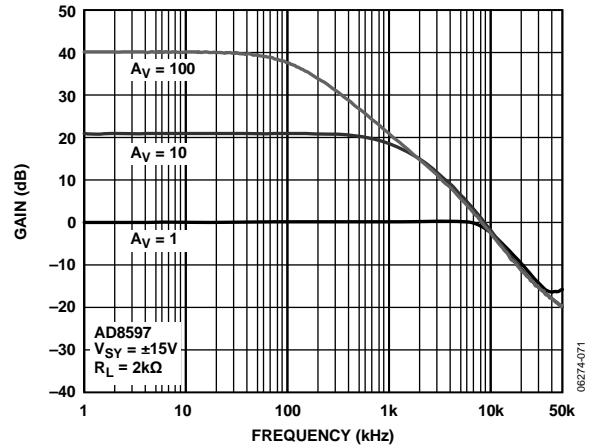


Figure 37. Closed-Loop Gain vs. Frequency

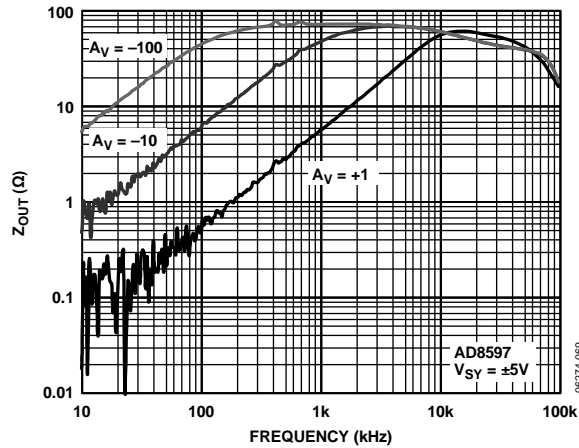


Figure 35. Closed-Loop Output Impedance vs. Frequency

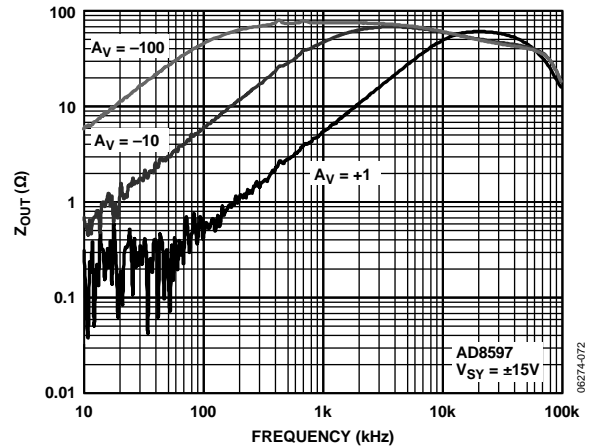


Figure 38. Closed-Loop Output Impedance vs. Frequency

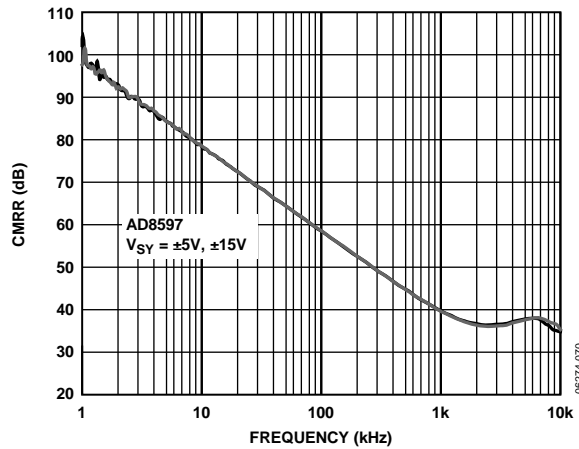


Figure 36. Common-Mode Rejection Ratio vs. Frequency

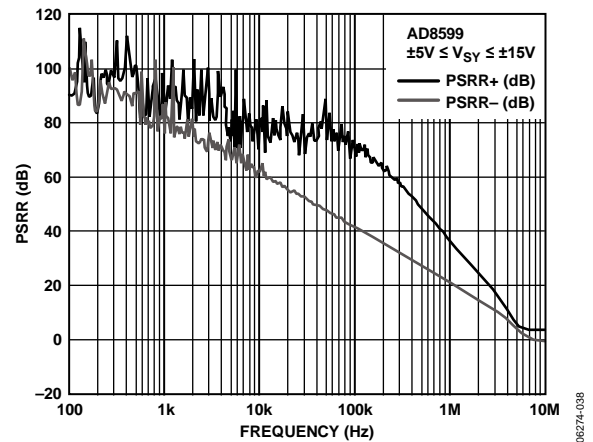


Figure 39. Power Supply Rejection Ratio vs. Frequency

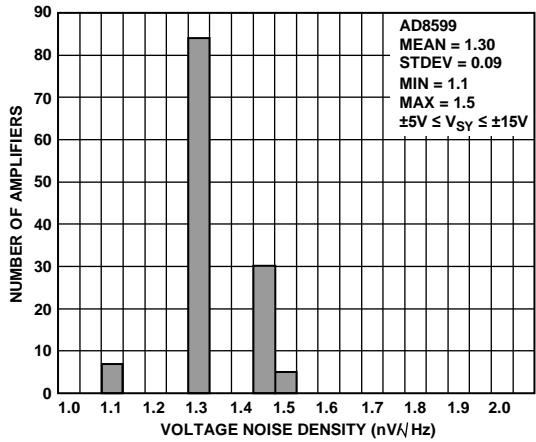


Figure 40. Voltage Noise Density @ 10 Hz

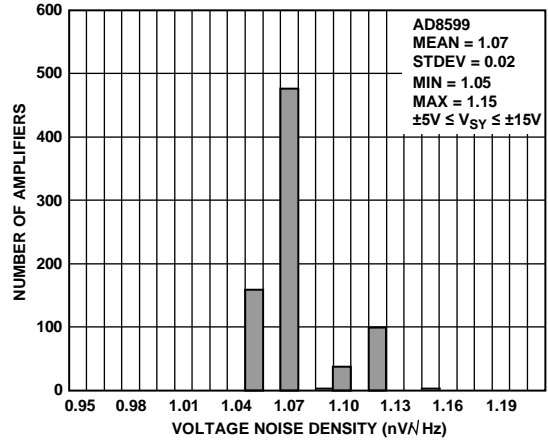


Figure 43. Voltage Noise Density @ 1 kHz

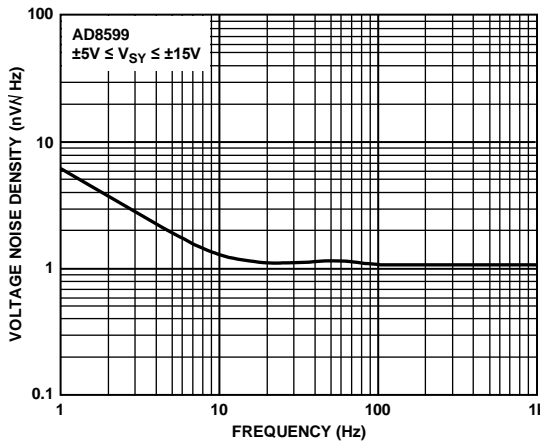


Figure 41. Voltage Noise Density vs. Frequency

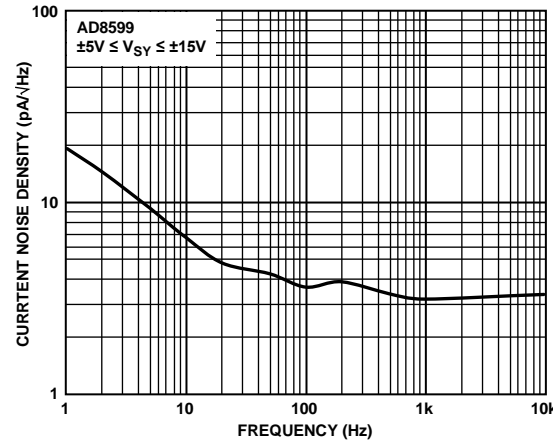


Figure 44. Current Noise Density vs. Frequency

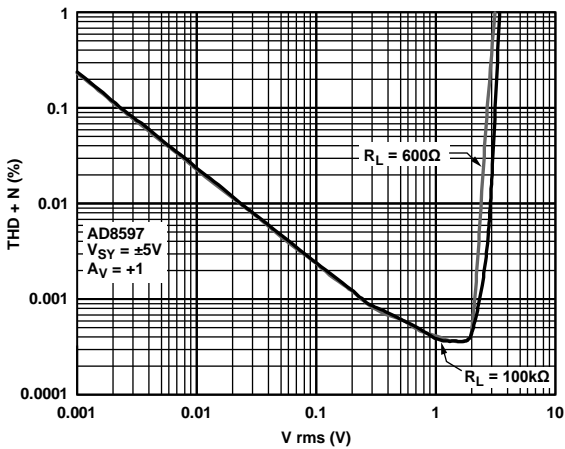


Figure 42. THD + N vs. Amplitude

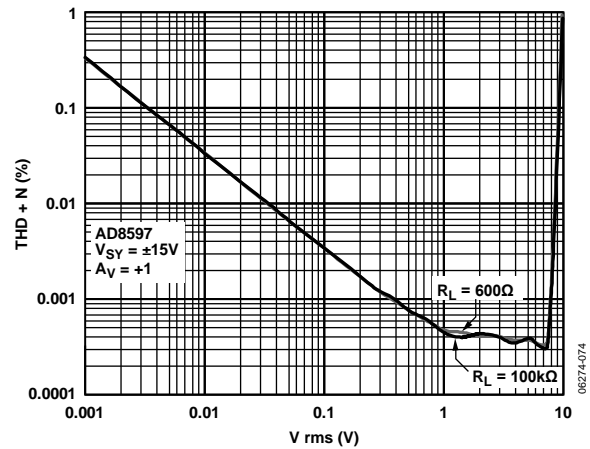


Figure 45. THD + N vs. Amplitude

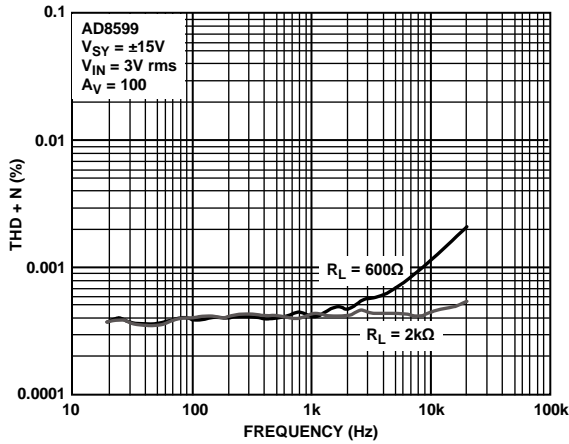


Figure 46. THD + N vs. Frequency

06274-043

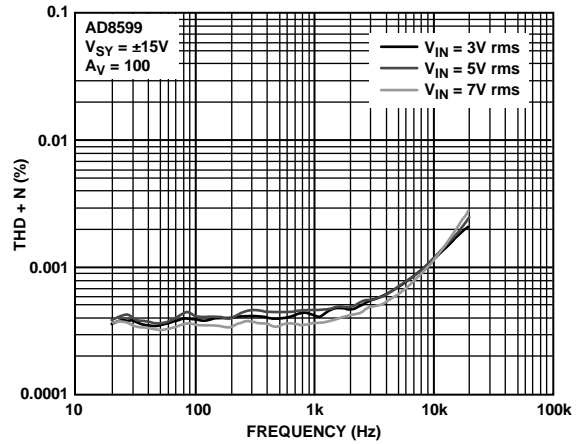


Figure 49. THD + N vs. Frequency

06274-044

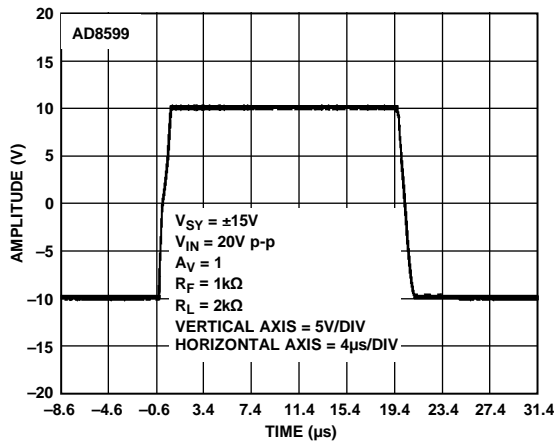


Figure 47. Large Signal Response

06274-047

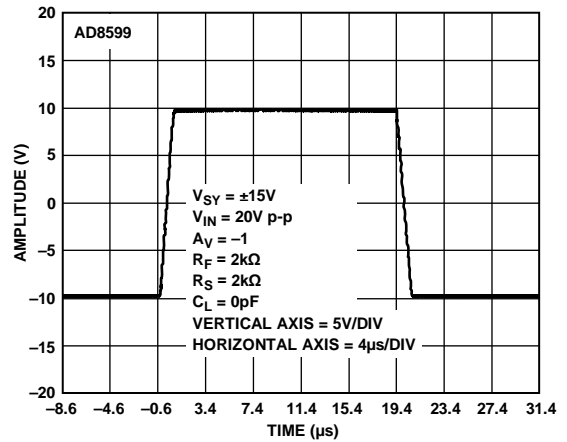


Figure 50. Large Signal Response

06274-048

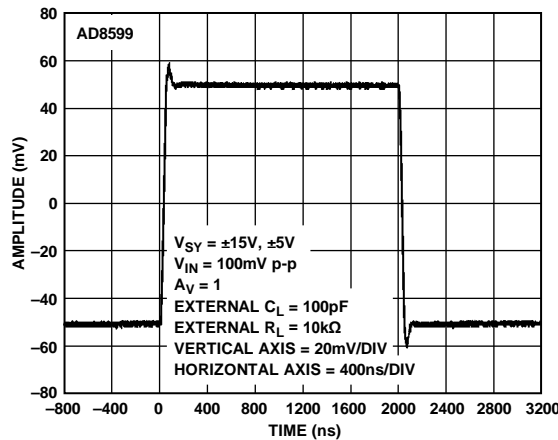


Figure 48. Small Signal Response

06274-046

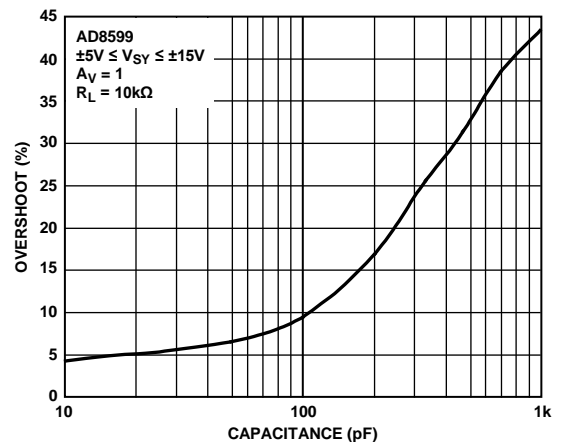


Figure 51. Overshoot vs. Capacitance

06274-049

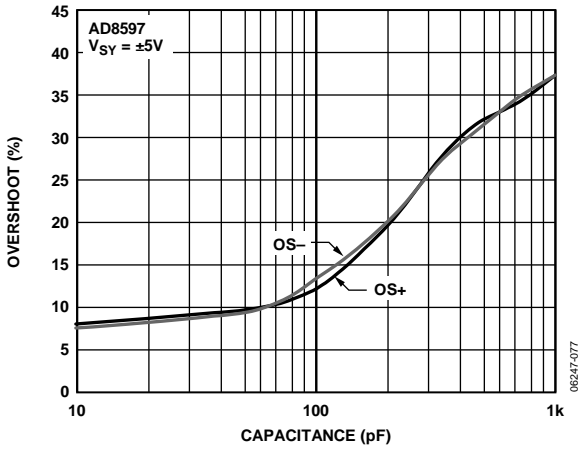


Figure 52. Overshoot vs. Capacitive Load

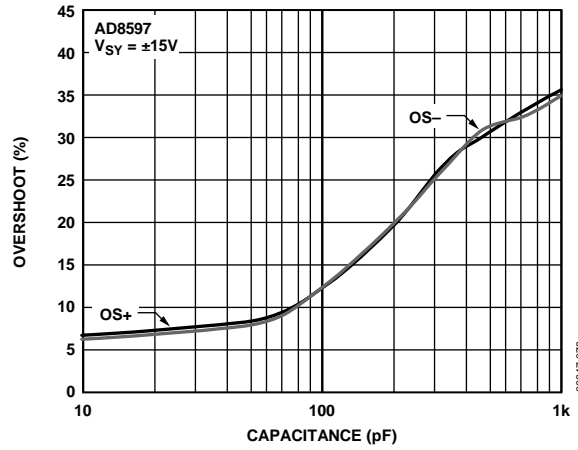


Figure 55. Overshoot vs. Capacitive Load

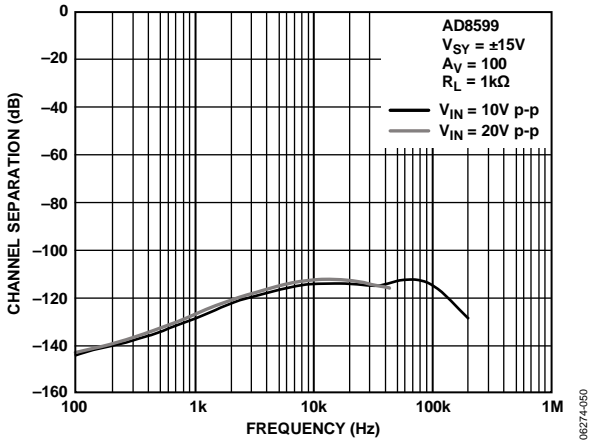


Figure 53. Channel Separation vs. Frequency

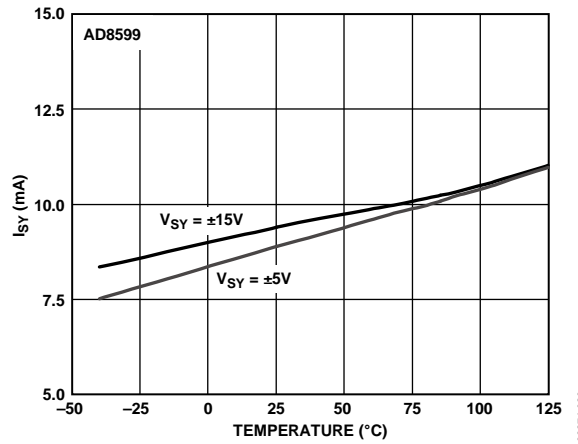


Figure 56. Supply Current vs. Temperature

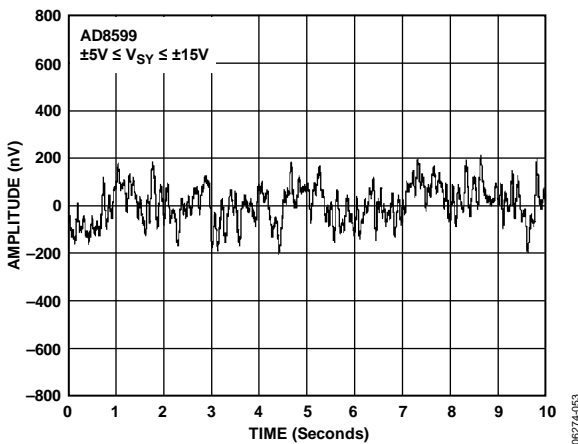


Figure 54. Peak-to-Peak Noise

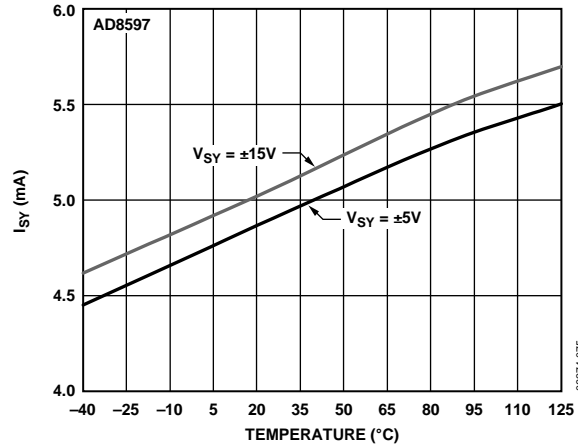


Figure 57. Supply Current vs. Temperature

## FUNCTIONAL OPERATION

### INPUT VOLTAGE RANGE

The AD8597/AD8599 are not rail-to-rail input amplifiers; therefore, care is required to ensure that both inputs do not exceed the input voltage range. Under normal negative feedback operating conditions, the amplifier corrects its output to ensure that the two inputs are at the same voltage. However, if either input exceeds the input voltage range, the loop opens and large currents begin to flow through the ESD protection diodes in the amplifier.

These diodes are connected between the inputs and each supply rail to protect the input transistors against an electrostatic discharge event and they are normally reverse-biased. However, if the input voltage exceeds the supply voltage, these ESD diodes can become forward-biased. Without current limiting, excessive amounts of current may flow through these diodes, causing permanent damage to the device. If inputs are subject to over-voltage, insert appropriate series resistors to limit the diode current to less than 5 mA maximum.

The input stage has two diodes between the input pins to protect the differential pair. Under high slew rate conditions, when the op amp is connected as a voltage follower, the diodes may become forward-biased and the source may try to drive the output. A small resistor should be placed in the feedback loop and in the noninverting input. The noise of a 100  $\Omega$  resistor at room temperature is  $\sim 1.25$  nV/ $\sqrt{\text{Hz}}$ , which is higher than the AD8597/AD8599. Thus, there is a tradeoff between noise performance and protection. If possible, limiting should be placed earlier in the signal path. For further details, see the *Amplifier Input Protection... Friend or Foe* article at [http://www.analog.com/amplifier\\_input](http://www.analog.com/amplifier_input).

Because of the large transistors used to achieve low noise, the input capacitance may seem rather high. To take advantage of the low noise performance, impedance around the op amp should be low, less than 500  $\Omega$ . Under these conditions, the pole from the input capacitance should be greater than 50 MHz, which does not affect the signal bandwidth.

### OUTPUT PHASE REVERSAL

Output phase reversal occurs in some amplifiers when the input common-mode voltage range is exceeded. As the common-mode voltage is moved outside the input voltage range, the outputs of these amplifiers can suddenly jump in the opposite direction to the supply rail. This is the result of the differential input pair shutting down that causes a radical shifting of internal voltages that results in the erratic output behavior.

The AD8597/AD8599 amplifiers have been carefully designed to prevent any output phase reversal if both inputs are maintained within the specified input voltage range. If one or both inputs exceed the input voltage range but remain within the supply rails, the op amp specifications, such as CMRR, are not guaranteed, but the output remains close to the correct value.

### NOISE AND SOURCE IMPEDANCE CONSIDERATIONS

The AD8597/AD8599 ultralow voltage noise of 1.1 nV/ $\sqrt{\text{Hz}}$  is achieved with special input transistors running at high collector current. Therefore, it is important to consider the total input-referred noise ( $e_N$  total), which includes contributions from voltage noise ( $e_N$ ), current noise ( $i_N$ ), and resistor noise ( $\sqrt{4 kTR_S}$ ).

$$e_N \text{ total} = [e_N^2 + 4 kTR_S + (i_N \times R_S)^2]^{1/2} \quad (1)$$

where  $R_S$  is the total input source resistance.

This equation is plotted for the AD8597/AD8599 in Figure 58. Because optimum dc performance is obtained with matched source resistances, this case is considered even though it is clear from Equation 1 that eliminating the balancing source resistance lowers the total noise by reducing the total  $R_S$  by a factor of 2.

At a very low source resistance ( $R_S < 50 \Omega$ ), the voltage noise of the amplifier dominates. As source resistance increases, the Johnson noise of  $R_S$  dominates until a higher resistance of  $R_S > 2 \text{ k}\Omega$  is achieved; the current noise component is larger than the resistor noise.

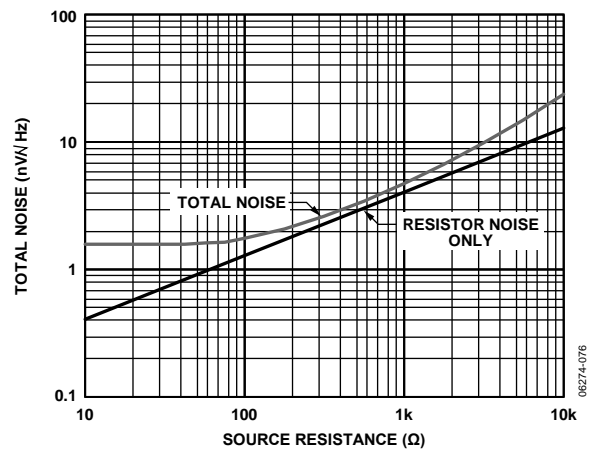


Figure 58. Noise vs. Source Resistance

The AD8597/AD8599 are the optimum choice for low noise performance if the source resistance is kept < 1 kΩ. At higher values of source resistance, optimum performance with respect to only noise is obtained with other amplifiers from Analog Devices. Both voltage noise and current noise need to be considered. For more information on avoiding noise from grounding problems and inadequate bypassing, see the AN-345 Application Note, *Grounding for Low- and High-Frequency Circuits*. For

general noise theory with extensive calculations, see the AN-358 Application Note, *Noise and Operational Amplifier Circuits*. A good selection table for low noise op amps can be found in AN-940 Application Note, *Low Noise Amplifier Selection Guide for Optimal Noise Performance*. An interesting note on using one section of a monolithic dual to phase compensate the other section is in the AN-107 Application Note, *Active Feedback Improves Amplifier Phase Accuracy*.

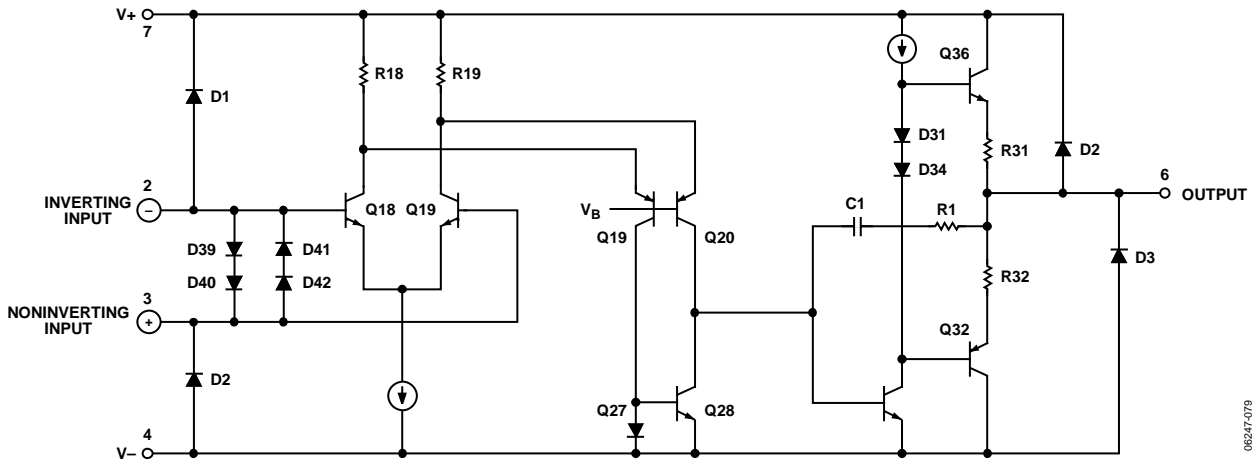
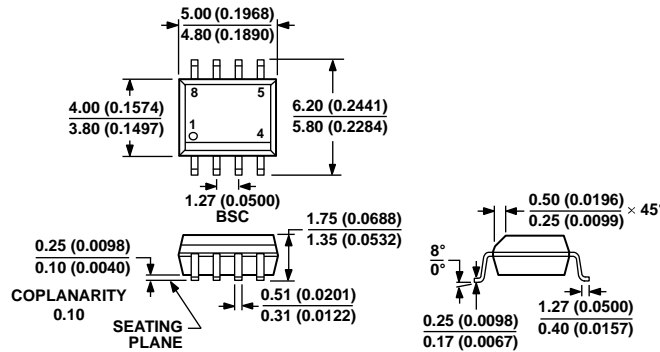


Figure 59. Simplified Schematic

66247-079



OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MS-012-AA  
 CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS  
 (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR  
 REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

Figure 60. 8-Lead Standard Small Outline Package [SOIC\_N]  
 Narrow Body (R-8)  
 Dimensions shown in millimeters and (inches)

012407-A

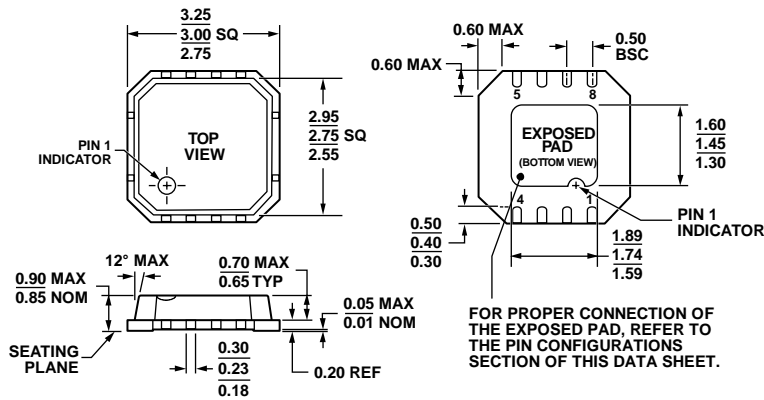


Figure 61. 8-Lead Lead Frame Chip Scale Package [LFCSP\_VD]  
 3 mm x 3 mm Body, Very Thin, Dual Lead  
 (CP-8-2)  
 Dimensions shown in millimeters

04-04-2012-A

ORDERING GUIDE

Model <sup>1</sup>	Temperature Range	Package Description	Package Option	Branding
AD8597ACPZ-R2	-40°C to +125°C	8-Lead Lead Frame Chip Scale Package [LFCSP_VD]	CP-8-2	A22
AD8597ACPZ-REEL	-40°C to +125°C	8-Lead Lead Frame Chip Scale Package [LFCSP_VD]	CP-8-2	A22
AD8597ACPZ-REEL7	-40°C to +125°C	8-Lead Lead Frame Chip Scale Package [LFCSP_VD]	CP-8-2	A22
AD8597ARZ	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	
AD8597ARZ-REEL	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	
AD8597ARZ-REEL7	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	
AD8599ARZ	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	
AD8599ARZ-REEL	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	
AD8599ARZ-REEL7	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	

<sup>1</sup> Z = RoHS Compliant Part.

**NOTES**

**NOTES**

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Компания «Life Electronics» занимается поставками электронных компонентов импортного и отечественного производства от производителей и со складов крупных дистрибьюторов Европы, Америки и Азии.

С конца 2013 года компания активно расширяет линейку поставок компонентов по направлению коаксиальный кабель, кварцевые генераторы и конденсаторы (керамические, пленочные, электролитические), за счёт заключения дистрибьюторских договоров

Мы предлагаем:

- Конкурентоспособные цены и скидки постоянным клиентам.
- Специальные условия для постоянных клиентов.
- Подбор аналогов.
- Поставку компонентов в любых объемах, удовлетворяющих вашим потребностям.
- Приемлемые сроки поставки, возможна ускоренная поставка.
- Доставку товара в любую точку России и стран СНГ.
- Комплексную поставку.
- Работу по проектам и поставку образцов.
- Формирование склада под заказчика.
- Сертификаты соответствия на поставляемую продукцию (по желанию клиента).
- Тестирование поставляемой продукции.
- Поставку компонентов, требующих военную и космическую приемку.
- Входной контроль качества.
- Наличие сертификата ISO.

В составе нашей компании организован Конструкторский отдел, призванный помогать разработчикам, и инженерам.

Конструкторский отдел помогает осуществить:

- Регистрацию проекта у производителя компонентов.
- Техническую поддержку проекта.
- Защиту от снятия компонента с производства.
- Оценку стоимости проекта по компонентам.
- Изготовление тестовой платы монтаж и пусконаладочные работы.



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